

LECTURE 18: adapted frame fields and connection forms on M

(1)

A frame on \mathbb{R}^3 was a set of 3 orthonormal vector fields $E_1, E_2, E_3 \in \Gamma(\mathbb{R}^3)$ now we adapt such a frame to fit with a given surface $M \subset \mathbb{R}^3$,

Defⁿ / An adapted frame field on $\mathcal{O} \subset M \subset \mathbb{R}^3$ is a Euclidean frame field such that $E_3(p) \in (T_p M)^\perp \forall p \in \mathcal{O}$.

We have $E_i \cdot E_j = \delta_{ij}$ so ~~any other~~ notation!
 $E_1, E_2, E_3(p) \in T_p M \quad \forall p \in \mathcal{O}$. If details of \mathcal{O} don't matter much to the discussion we'll just say E_1, E_2, E_3 is frame on M

Lemma 1.2: there is an adapted frame field on $\mathcal{O} \subset M$ $\Leftrightarrow \mathcal{O}$ is orientable and \exists a non vanishing tangent-vec field on \mathcal{O} .

Proof: \Rightarrow $\exists E_1, E_2, E_3$ is adapted frame field on $\mathcal{O} \subset M$.

Then E_3 serves as non vanishing normal to $\mathcal{O} \therefore \mathcal{O}$ oriented.
Moreover, E_1, E_2 are non vanishing tangent fields.

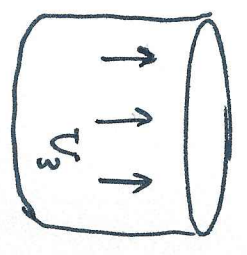
\Leftarrow \mathcal{O} orientable $\Rightarrow \exists \mathcal{U}$ a unit-normal on \mathcal{O} . Let $E_3 = \mathcal{U}$.
Also we assume $\exists E_2$ a non vanishing tang. field on \mathcal{O} .

Define $E_1 = E_2 \times E_3$ then it follows E_1, E_2, E_3 forms the desired frame field on $\mathcal{O} \subset M \subset \mathbb{R}^3$.

Remark: the technique of the proof is sometimes useful to construct frame fields on a given M .

Ex (1): CYLINDER $M : x^2 + y^2 = R^2$

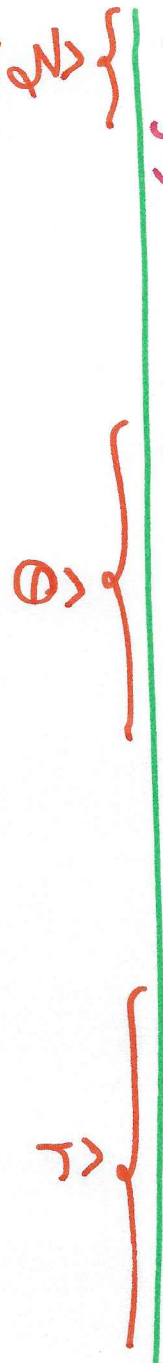
$\nabla(x^2 + y^2) = \langle 2x, 2y, 0 \rangle \implies \underline{E_3 = \frac{1}{R}(xU_1 + yU_2)}$




Notice $U_3 \cdot E_3 = 0 \implies \underline{E_1 = U_3}$ gets us tang.-field to M

Finally, $E_2 = E_3 \times E_1 = \frac{1}{R}(xU_1 \times U_3 + yU_2 \times U_3) = \underline{\underline{\frac{-x}{R}U_2 + \frac{y}{R}U_1}}$

Thus $E_1 = U_3, E_2 = \frac{y}{R}U_1 - \frac{x}{R}U_2, E_3 = \frac{1}{R}(xU_1 + yU_2)$



Multivariable calculus
I'd use notation  for this frame field.

(oh, this is the cylindrical frame restricted to $r=R$)

Remark: setting $E_2 = E_3 \times E_1$, for given $E_1 \neq E_3$

forces $E_1 \times E_2 = E_3$ and $E_2 \times E_3 = E_1$. In short it's a

RIGHT-HANDED FRAME

Ex (2) SPHERE $\Sigma^1 : x^2 + y^2 + z^2 = R^2$

(3)

$E_3 = \frac{1}{R} (x U_1 + y U_2 + z U_3)$ ← $\frac{\nabla(x^2+y^2+z^2)}{\|\nabla(x^2+y^2+z^2)\|}$ normalized gradient

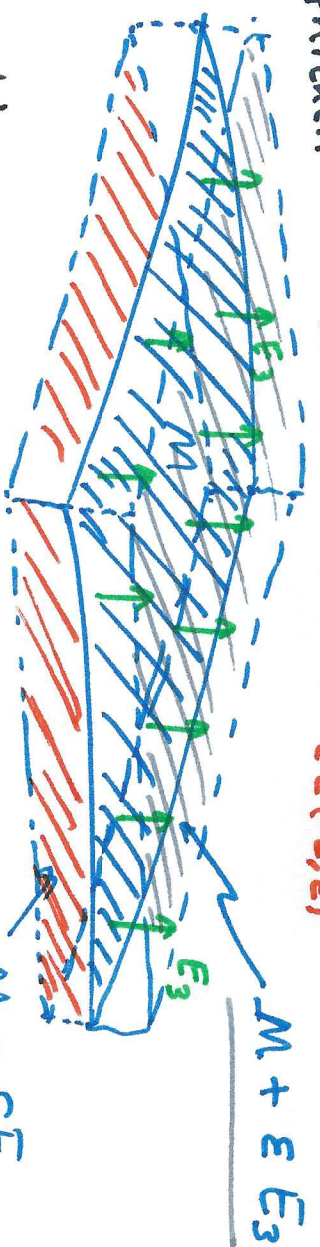
" $\hat{\theta}$ ": $E_{\hat{\theta}} = \frac{-y U_1 + x U_2}{\sqrt{x^2+y^2}}$: clearly $E_{\hat{\theta}} \cdot E_3$ and $\|E_{\hat{\theta}}\| = 1$ except at N/S pole where $x=y=0$.

$E_2 = \underbrace{E_3 \times E_1}_{\hat{\theta} \times \hat{\theta}} = \frac{1}{R\sqrt{x^2+y^2}} (-x z U_1 - y z U_2 + (x^2+y^2) U_3)$

(in my usual vector calculus notation I can't help but comment)

Remark: in spherical coord. there are prettier, but, I shall not digress further..

• Our results for frame fields on \mathbb{R}^3 or open sets in \mathbb{R}^3 don't directly apply since M is not an open set in \mathbb{R}^3 . HOWEVER, as Shlomo Sternberg illustrates in his text on CURVATURE we can thicken M to a RIBBON $U(M+cE_3)$ roughly.



then connection equations hold for RIBBON and we can restrict these back to M once again

$M - \epsilon E_3$

$M + \epsilon E_3$

CONNECTION EQUATIONS ON SURFACE

$\nabla_v E_i$ If E_1, E_2, E_3 is an adapted frame on M then $\nabla_v E_i = \sum_{j=1}^3 \omega_{ij}(v) E_j(p)$ for $i=1,2,3$ and all $v \in T_p M$

Recall, from S 2.7 p. 88,
 $\omega_{ij}(v) = (\nabla_v E_i) \cdot E_j$

In view of the defⁿ of ω_{ij} this theorem just expresses orthonormal expansion of $\nabla_v E_i$ in terms of E_1, E_2, E_3 frame.

Comment: $\omega_{ij}(v)$ tells us the rate at which E_i (initially) rotates toward E_j as p moves in the v -direction.

Proposition: for the shape operator S^t at p and $v \in T_p M$,
 $S(v) = \omega_{13}(v) E_1(p) + \omega_{23}(v) E_2(p)$

Proof: $v = E_3$ for M thus $S(v) = -\nabla_v v = -\nabla_v E_3$.

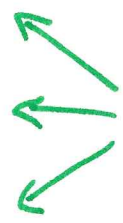
Recall $\omega_{ij} = -\omega_{ji}$ thus $\nabla_v E_3 = \omega_{31}(v) E_1 + \omega_{32}(v) E_2 + \cancel{\omega_{33}(v) E_3}$

$\therefore S(v) = \omega_{13}(v) E_1 + \omega_{23}(v) E_2$

where we've used $\omega_{13} = -\omega_{31}$, & $\omega_{23} = -\omega_{32}$ to absorb (-). //

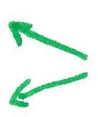
Coframe on M

E_1, E_2, E_3 adapted to M , only E_1, E_2 are tangent to M



$\theta^1, \theta^2, \theta^3$

coframe $\theta^i(E_j) = \delta_{ij}$



θ^1, θ^2 one-forms on M

$\theta^3 \equiv 0$ on M .

θ^3 kills any lin. combo of $E_1, \theta E_2$ hence all of $T_p M$ for each P .

We study the following

θ^1, θ^2 dual to E_1, E_2

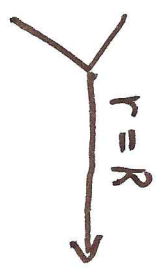
W_{12} gives how E_1 rotates to E_2

W_{13}, W_{23} capture shape operator as given by E_3

~~(this is covered in pages to come...)~~

Example: dual to cylindrical frame (Ex 2.7.6 my notes)

$\theta^1 = dr$
 $\theta^2 = r d\theta$
 $\theta^3 = dz$



$\theta^1 \equiv 0$
 $\theta^2 = R d\theta$
 $\theta^3 = dz$

So, the label doesn't fit with our E_3 is normal... this is why we sometimes begin by relabeling old example \rightarrow

Ex: Cotframe to Cylinder

$$\begin{aligned}\theta^1 &= r d\theta \\ \theta^2 &= dz \\ \theta^3 &= dr\end{aligned}$$

$$\xrightarrow{r=R}$$

$\theta^1 = R d\theta$
$\theta^2 = dz$

adjusted Ex. 2.7.6 my notes.

Ex: cotframe to sphere

$$\begin{aligned}\theta^1 &= \rho d\phi \\ \theta^2 &= \rho \sin\phi d\theta \\ \theta^3 &= d\rho\end{aligned}$$

$$\xrightarrow{\rho=R}$$

$\theta^1 = R d\phi$
$\theta^2 = R \sin\phi d\theta$

adjusted Ex. 2.7.7 my notes.

7.3 CARTAN'S STRUCTURE EQUATIONS ADAPTED TO M

Suppose E_1, E_2, E_3 is an adapted frame on $M \subset \mathbb{R}^3$
 then its dual-forms θ^1, θ^2 and connection-forms ω_{ij} on M satisfy:

(1) $\left[\begin{matrix} d\theta^1 = \omega_{12} \wedge \theta^2 \\ d\theta^2 = \omega_{21} \wedge \theta^1 \end{matrix} \right]$ — 1st structural eq's ← $d\theta = \omega \wedge \theta$

(2) $[\omega_{31} \wedge \theta^1 + \omega_{32} \wedge \theta^2 = 0]$ — symmetry eq's ← $d\theta^3 = \omega_{31} \wedge \theta^1 + \omega_{32} \wedge \theta^2$

(3.) $[d\omega_{12} = \omega_{13} \wedge \omega_{32}]$ — Gauss' eq's

(4.) $\left[\begin{matrix} d\omega_{13} = \omega_{12} \wedge \omega_{23} \\ d\omega_{23} = \omega_{21} \wedge \omega_{13} \end{matrix} \right]$ — Codazzi eq's.

$\left\{ \begin{matrix} \text{tells us how} \\ \text{shape of } M \\ \text{changes from} \\ \text{point to point} \\ \text{since } S \text{ is} \\ \text{determined by} \\ \omega_{13} \text{ \& } \omega_{23} \end{matrix} \right.$

Proof: there are just $d\theta = \omega \wedge \theta$ and $d\omega = \omega \wedge \omega$
 with $\theta^3 \equiv 0$ from our previous work in Chapter 2.

Application: $\theta^1 = R d\phi \rightarrow d\theta^1 = 0$
 following $\theta^2 = R \sin\phi d\theta \rightarrow d\theta^2 = R \cos\phi d\phi \wedge d\theta$

Now, $d\theta^2 = \omega_{21} \wedge \theta^1 = \omega_{21} \wedge (R d\phi) = R \cos\phi d\phi \wedge d\theta$
 $d\theta^1 = \omega_{12} \wedge \theta^2$
 $0 = \omega_{12} \wedge (R \sin\phi d\theta) \Rightarrow \omega_{21} = -\cos\phi d\theta \therefore \omega_{12} = \cos\phi d\theta$

Remark: This is based on Ex. 2.7.7 of my notes with $\begin{bmatrix} 1 & \rightarrow & 3 \\ 2 & \rightarrow & 1 \\ 3 & \rightarrow & 2 \end{bmatrix}$, this is ω_{23} in Ex. 2.7.7, or if ought.

§ 6.2 Form Computations

VECTOR FIELD V on M ; $V = (V \cdot E_1)E_1 + (V \cdot E_2)E_2$

ONE-FORM α on M ; $\alpha = \alpha(E_1)\theta^1 + \alpha(E_2)\theta^2$

TWO-FORM μ on M ; $\mu = \mu(E_1, E_2)\theta^1 \wedge \theta^2$

The claims above follow from def^s we gave in Chapter 4 as well as the duality condition $\theta^i(E_j) = \delta_{ij}$.

Example Proof: θ^1, θ^2 basis here $\alpha = c_1\theta^1 + c_2\theta^2$. But,

$$\alpha(E_1) = c_1 \cancel{\theta^1(E_1)} + c_2 \cancel{\theta^2(E_1)} = c_1 \quad \text{and} \quad \alpha(E_2) = c_1 \cancel{\theta^1(E_2)} + c_2 \cancel{\theta^2(E_2)} = c_2$$

Thus $\alpha = \alpha(E_1)\theta^1 + \alpha(E_2)\theta^2$ as claimed.

Lemma 2.2: $\begin{cases} (1) & W_{13} \wedge W_{23} = K \theta_1 \wedge \theta_2 \\ (2) & W_{13} \wedge \theta_2 + \theta_1 \wedge W_{23} = 2H \theta_1 \wedge \theta_2 \end{cases}$

Proof: $W_{13} \wedge W_{23} = (W_{13}(E_1)\theta^1 + W_{13}(E_2)\theta^2) \wedge (W_{23}(E_1)\theta^1 + W_{23}(E_2)\theta^2)$
 $= [W_{13}(E_1)W_{23}(E_2) - W_{13}(E_2)W_{23}(E_1)] \theta^1 \wedge \theta^2$
 $= (\det S) \theta^1 \wedge \theta^2$: By Lemma \checkmark
 $= K \theta^1 \wedge \theta^2$

Lemma: $\det S = w_{13}(E_1)w_{23}(E_2) - w_{13}(E_2)w_{23}(E_1)$

Proof: we wish to express $\det S$ in terms of frame E_1, E_2 .

We have $S(V) = w_{13}(V)E_1 + w_{23}(V)E_2$ hence

$$\begin{bmatrix} S(E_1) = w_{13}(E_1)E_1 + w_{23}(E_1)E_2 \\ S(E_2) = w_{13}(E_2)E_1 + w_{23}(E_2)E_2 \end{bmatrix} \rightarrow [S] = \begin{bmatrix} w_{13}(E_1) & w_{13}(E_2) \\ w_{23}(E_1) & w_{23}(E_2) \end{bmatrix}$$

Therefore, $\det(S) = w_{13}(E_1)w_{23}(E_2) - w_{13}(E_2)w_{23}(E_1)$ as claimed.

Continue to prove (2): $w_{13} \wedge \theta^2 + \theta^1 \wedge w_{23} = 2H \theta^1 \wedge \theta^2$

$$\begin{aligned} w_{13} \wedge \theta^2 + \theta^1 \wedge w_{23} &= (w_{13}(E_1)\theta^1 + w_{13}(E_2)\theta^2) \wedge \theta^2 + \theta^1 \wedge (w_{23}(E_1)\theta^1 + w_{23}(E_2)\theta^2) \\ &= [w_{13}(E_1) + w_{23}(E_2)] \theta^1 \wedge \theta^2 \\ &= \text{trace}(S) \theta^1 \wedge \theta^2 \\ &= \underline{2H \theta^1 \wedge \theta^2} \quad // \end{aligned}$$

Corollary (2.3): $dw_{12} = -K \theta^1 \wedge \theta^2$

\leftarrow 2nd structural Eq.

Proof: $dw_{12} = w_{13} \wedge w_{32} = -w_{12} \wedge w_{23} = -K \theta^1 \wedge \theta^2$

$\underbrace{\hspace{10em}}_{\text{Gauss Eq.}}$

Application: calculate K for sphere.

$$\left. \begin{aligned} \Theta^1 &= R d\phi \\ \Theta^2 &= R \sin\phi d\theta \end{aligned} \right\} \longrightarrow \Theta^1 \wedge \Theta^2 = R^2 \sin\phi d\phi \wedge d\theta \quad \text{(no need for } \Theta^3 \text{)}$$

$$W_{12} = \cos\phi d\theta \longrightarrow dW_{12} = -\sin\phi d\phi \wedge d\theta$$

$$\text{Then } \omega \quad dW_{12} = -K \Theta^1 \wedge \Theta^2 \longrightarrow -\sin\phi d\phi \wedge d\theta = -K R^2 \sin\phi d\phi \wedge d\theta$$

"2nd Structural Eqⁿ" \therefore $K = 1/R^2$

Defⁿ / A PRINCIPAL FRAME FIELD on $M \subset \mathbb{R}^3$ is an adapted frame field E_1, E_2, E_3 such that E_1, E_2 are everywhere principal vectors on M .

For nonumbilic points this determines a particular choice of frame (modulo sign choice). As O'Neill points out for S.O. Rev. the tangents to meridians and parallels.

Lemma (2.5): If P is a nonumbilic point of $M \subset \mathbb{R}^3$ then \exists a principal frame field on some nbhd of P in M .

Proof: if P is nonumbilic $\Rightarrow h(u)$ is non-constant at $P \Rightarrow h_1(P) \neq h_2(P)$
 or, $(h_1 - h_2)(P) \neq 0$. By continuity, \exists nbhd of P for which all $q \in$ nbhd have $(h_1 - h_2)(q) \neq 0$. Then the normalized e-vect. of S on nbhd give the frame.
 (shipped some detail here see 271-272)

Let E_1, E_2, E_3 be a principal frame field, thus \exists functions k_1, k_2 and K_1, K_2 for which $S(E_1) = k_1 E_1$, $\neq S(E_2) = k_2 E_2$

$$S(E_1) = \underline{w_{13}(E_1)} E_1 + \underline{w_{23}(E_1)} E_2 = \underline{k_1} E_1 + \underline{0} \cdot E_2$$

$$S(E_2) = \underline{w_{13}(E_2)} E_1 + \underline{w_{23}(E_2)} E_2 = \underline{k_2} E_2 + \underline{0} \cdot E_1$$

Thus we derive,

$$w_{13}(E_1) = k_1 \quad \neq \quad w_{13}(E_2) = 0 \quad \therefore$$

$$\boxed{w_{13} = k_1 \theta^1}$$

$$w_{23}(E_1) = 0 \quad \neq \quad w_{23}(E_2) = k_2 \quad \therefore$$

$$\boxed{w_{23} = k_2 \theta^2}$$

Th^m / If E_1, E_2, E_3 is principal frame on M then $\begin{cases} E_1[k_2] = (k_1 - k_2) w_{12}(E_2) \\ E_2[k_1] = (k_1 - k_2) w_{12}(E_1) \end{cases}$

Proof: We have $d w_{13} = w_{12} \wedge w_{23} \Rightarrow d(k_1 \theta^1) = w_{12} \wedge (k_2 \theta^2)$

$$\therefore dk_1 \wedge \theta^1 + k_1 d\theta^1 = w_{12} \wedge (k_2 \theta^2) \quad \text{and so } d\theta^1 = w_{12} \wedge \theta^2$$

$$\Rightarrow dk_1 \wedge \theta^1 + k_1 w_{12} \wedge \theta^2 = k_2 w_{12} \wedge \theta^2$$

$$\Rightarrow dk_1 \wedge \theta^1 = (k_2 - k_1) w_{12} \wedge \theta^2$$

$$\Rightarrow dk_1 [E_2] \theta^2 \wedge \theta^1 = (k_2 - k_1) (w_{12} [E_1] \theta^1 + w_{12} [E_2] \theta^2) \wedge \theta^2$$

could have omitted this 😊

$$\Rightarrow -dk_1(E_2) \theta^1 \wedge \theta^2 = (k_2 - k_1) w_{12}(E_1) \theta^1 \wedge \theta^2$$

$$\boxed{\star}$$



$$dk_1 = dk_1 [E_1] \theta^1 + dk_1 [E_2] \theta^2$$

Continuing, comparing coeff. of $\theta' \wedge \theta^2$ yields,

$$-dh_1(\bar{E}_2) = (k_2 - h_1)w_{12}(\bar{E}_1)$$

$$\Rightarrow \underline{E_2[k_1] = (h_1 - k_2)w_{12}(\bar{E}_1)} //$$

Likewise, $dw_{23} = w_{21} \wedge w_{13}$

$$d(h_2 \theta^2) = -w_{12} \wedge (h_1 \theta^1)$$

$$dh_2 \wedge \theta^2 + h_2 d\theta^2 = -k_1 w_{12} \wedge \theta^1$$

$$dh_2 \wedge \theta^2 + h_2 w_{21} \wedge \theta^1 = -k_1 w_{12} \wedge \theta^1$$

$$dh_2 \wedge \theta^2 = (-k_1 + h_2)w_{12} \wedge \theta^1$$

$$dh_2[E_1] \theta^1 \wedge \theta^2 = (k_2 - h_1)w_{12}[E_2] \theta^2 \wedge \theta^1$$

$$\therefore dh_2[E_1] = (h_1 - k_2)w_{12}[E_2]$$

$$\underline{E_1[k_2] = (h_1 - k_2)w_{12}[E_2]} //$$

Remark: This theorem shows for principal frame w_{12} controls how principal curvatures h_1, k_2 change in principal directions E_1, E_2 .