

$1\text{mm} = 10^{-3}\text{m}$   
 $1\text{Å} = 10^{-10}\text{m}$

atomic radius =  $r = \frac{1}{2}\text{Å}$

20/20

$\alpha = 0.667(4\pi\epsilon_0)$   
 $q = e = 1.602 \times 10^{-19}\text{C}$

If the plates are quite large the the  $\vec{E}$  is essential uniform between the plates and we remember that

$V = Ex \Rightarrow E = \frac{V}{x}$  where  $\begin{cases} V = 500\text{V} \\ x = 1\text{mm} \end{cases}$

$P = qd = \alpha E = \alpha \frac{V}{x} \Rightarrow d = \frac{\alpha V}{q x}$ ,  $\alpha = (0.667) 4\pi\epsilon_0$

$\frac{d}{\text{atomic radius}} = \frac{d}{\frac{1}{2}\text{Å}} = \frac{\frac{\alpha V}{q x}}{\frac{1}{2}\text{Å}} = \frac{(0.667)(4\pi\epsilon_0)(500\text{V})(10^{-30})}{(1.602 \times 10^{-19}\text{C})(0.001\text{m})(0.5 \times 10^{-10}\text{m})} = 4.63 \times 10^{-6}$

fraction  $\approx \frac{1}{215,000}$  of an atomic radius ✓

$d = 2.3 \times 10^{-16}\text{m}$

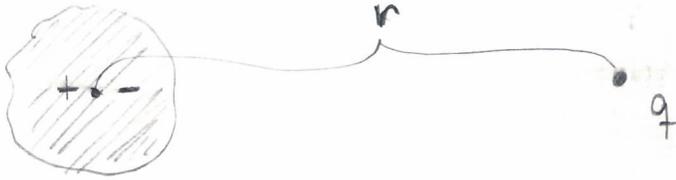
(b) estimate potential necessary to ionize atom, to remove the electron from Bohr's model atom all we need is to separate the electron by  $r$  from the center that is

$d = r$ ,  $P = qd = \alpha E = \alpha \frac{V}{x} \Rightarrow q r = \frac{\alpha V}{x}$

$V = \frac{x q r}{\alpha} = \frac{(0.001\text{m})(1.602 \times 10^{-19}\text{C})(10^{-10}\text{m})^{\frac{1}{2}}}{(4\pi\epsilon_0)(0.667)(10^{-30})} = 108\text{MV}$  ✓  
 $1.1 \times 10^8\text{V}$

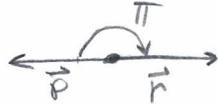
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4-4 A point charge  $q$  is situated  $r$  away from a neutral atom of polarizability  $\alpha$ . Find force of attraction between them.



$$\vec{E}_q = \frac{1}{4\pi\epsilon_0} \frac{q}{r^2} \hat{r}$$

$$p = \alpha E_q = \frac{\alpha}{4\pi\epsilon_0} \frac{q}{r^2}$$



$$\vec{E}_{dip} = \frac{p}{4\pi\epsilon_0 r^3} (2\cos\theta \hat{r} + \sin\theta \hat{\theta})$$

$$= \frac{p}{4\pi\epsilon_0 r^3} (-2\cos(\pi)) \hat{r}$$

$$= \frac{-2}{4\pi\epsilon_0 r^3} \left( \frac{\alpha}{4\pi\epsilon_0} \frac{q}{r^2} \right) \hat{r}$$

$$= \frac{-2\alpha q}{(4\pi\epsilon_0)^2 r^5} \hat{r}$$

$$= \frac{-\alpha q}{8\pi^2 \epsilon_0^2 r^5} \hat{r}$$

See solution for alternate method.

$$\vec{F} = q \vec{E}_{dip} = \boxed{\frac{-\alpha q^2}{8\pi^2 \epsilon_0^2 r^5} \hat{r} = \vec{F}}$$

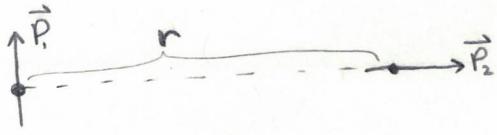
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$$F = -\frac{2\alpha q^2}{(4\pi\epsilon_0)^2 r^5} \hat{r}$$

4-5

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$$\vec{E}_{dip} = \frac{p}{4\pi\epsilon_0 r^3} (3(\vec{p} \cdot \hat{r})\hat{r} - \vec{p})$$

19/20

a) What is Torque on  $\vec{P}_2$  from  $\vec{P}_1$

$$\vec{P}_1 = P_1 \hat{j}, \quad \vec{E}_1 = \frac{1}{4\pi\epsilon_0 r^3} (3(P_1 \hat{j} \cdot \hat{i})\hat{i} - P_1 \hat{j}) = \frac{1}{4\pi\epsilon_0 r^3} (-P_1 \hat{j}) = \frac{-P_1}{4\pi\epsilon_0 r^3} \hat{j}$$

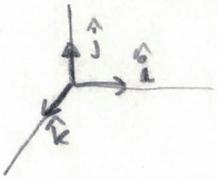
$$\vec{N}_{21} = \vec{P}_2 \times \vec{E}_1 = (P_2 \hat{i}) \times \left( \frac{-P_1}{4\pi\epsilon_0 r^3} \hat{j} \right) = \frac{-P_1 P_2}{4\pi\epsilon_0 r^3} (\hat{i} \times \hat{j}) = \boxed{\frac{-P_1 P_2}{4\pi\epsilon_0 r^3} \hat{k}}$$

(b) What is Torque on  $\vec{P}_1$  from  $\vec{P}_2$

$$\vec{P}_2 = P_2 \hat{i}, \quad \vec{E}_2 = \frac{1}{4\pi\epsilon_0 r^3} (3(P_2 \hat{i} \cdot (-\hat{i}))(-\hat{i}) - P_2 \hat{i}) = \frac{1}{4\pi\epsilon_0 r^3} (3P_2 \hat{i} - P_2 \hat{i}) = \frac{2P_2}{4\pi\epsilon_0 r^3} \hat{i}$$

$$\vec{N}_{12} = \vec{P}_1 \times \vec{E}_2 = (P_1 \hat{j}) \times \left( \frac{2P_2}{4\pi\epsilon_0 r^3} \hat{i} \right) = \boxed{\frac{-2P_1 P_2}{4\pi\epsilon_0 r^3} \hat{k}}$$

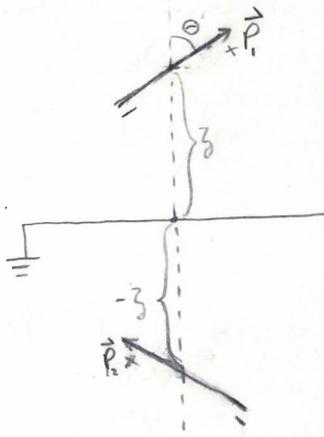
note



so my  $\vec{N}$ 's go into the page

↻

4-6



Using the method of images we situate the second pretend dipole below the plane to cancel real dipole.

$$\vec{p}_1 = p \cdot \cos\theta \hat{z} + p \sin\theta \hat{x}$$

$$\vec{p}_2 = p \cos\theta \hat{z} - p \sin\theta \hat{x}$$

$$\vec{E}_2 = \frac{1}{4\pi\epsilon_0 (2z)^3} (3(\vec{p}_2 \cdot \hat{z})\hat{z} - \vec{p}_2) = \frac{1}{4\pi\epsilon_0 (2z)^3} (3[p \cos\theta \hat{z} - p \sin\theta \hat{x}] \cdot \hat{z} \hat{z} - \vec{p}_2)$$

$$= \frac{p}{32\pi\epsilon_0 z^3} (3 \cos\theta \hat{z} - \cos\theta \hat{z} + \sin\theta \hat{x})$$

$$= \frac{p}{32\pi\epsilon_0 z^3} (2 \cos\theta \hat{z} + \sin\theta \hat{x})$$

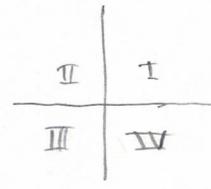
$$\vec{N} = \vec{p}_1 \times \vec{E}_2 = (\cos\theta \hat{z} + \sin\theta \hat{x}) \times (2 \cos\theta \hat{z} + \sin\theta \hat{x}) \left[ \frac{p^2}{32\pi\epsilon_0 z^3} \right]$$

$$= \left[ \cos\theta (2 \cos\theta) \hat{z} \times \hat{z} + (\cos\theta \sin\theta) \hat{z} \times \hat{x} + (\sin\theta (2 \cos\theta)) \hat{x} \times \hat{z} + (\sin\theta \sin\theta) \hat{x} \times \hat{x} \right] \left[ \frac{p^2}{32\pi\epsilon_0 z^3} \right]$$

$$= \left[ -\sin\theta \cos\theta \hat{y} + 2 \sin\theta \cos\theta \hat{y} \right] \left[ \frac{p^2}{32\pi\epsilon_0 z^3} \right]$$

$$= \frac{p^2}{32\pi\epsilon_0 z^3} (\sin\theta \cos\theta) \hat{y}$$

$$\vec{N} = \frac{p^2 \sin 2\theta}{4 \cdot 16\pi\epsilon_0 z^3} \hat{y}$$



$\vec{N} = 0$  for  $\theta = 0, \frac{\pi}{2}, \pi$

Say  $\vec{p}$  starts in quadrant I then  $\vec{N}$  is  $\hat{y}$  causing CCW rot once  $\vec{p}$  goes to II then  $\vec{N}$  is negative ( $\theta = 0 \rightarrow -\pi/2$ ) so it causes a CW rotation back then a CCW then a CW ... It seems it will come to rest pointed upwards if it starts oriented as it drawn in the books diagram

*N is largest at  $\pi/4$*

9

4.12

PY 914, DR. CHUNG.

JAMES COOK

$$V = \frac{1}{4\pi\epsilon_0} \int \frac{\vec{P} \cdot \hat{n}}{r^2} dt' = \frac{\vec{P}}{4\pi\epsilon_0} \cdot \int \frac{\hat{n}}{r^2} dt' \quad \text{20/19/20}$$

Use trick to get.

$$\vec{E} = \frac{1}{4\pi\epsilon_0} \frac{Q\vec{r}}{R^3} \quad \vec{E} = \frac{1}{4\pi\epsilon_0} \int \frac{\rho \hat{n}}{r^2} dt' = \frac{\rho}{4\pi\epsilon_0} \int \frac{\hat{n}}{r^2} dt'$$

(Uniformly charged sphere)

$$= \frac{1}{4\pi\epsilon_0} \frac{Q}{\frac{4}{3}\pi R^3} \int \frac{\hat{n}}{r^2} dt' \quad \text{(Coulomb's law)}$$

$$\vec{E} = \frac{1}{4\pi\epsilon_0} \frac{Q\vec{r}}{R^3} = \frac{1}{4\pi\epsilon_0} \frac{Q}{\frac{4}{3}\pi R^3} \int \frac{\hat{n}}{r^2} dt'$$

$$\Rightarrow \int \frac{\hat{n}}{r^2} dt' = \frac{Q\vec{r}}{R^3} \frac{\frac{4}{3}\pi R^3}{Q} = \vec{r} \frac{4}{3}\pi \quad \text{the trick is complete}$$

$$V = (\vec{P} \cdot \vec{r}) \frac{4}{3}\pi \left( \frac{1}{4\pi\epsilon_0} \right) = \frac{\vec{P} \cdot \vec{r}}{3\epsilon_0} = \boxed{\frac{Pr \cos \theta}{3\epsilon_0} = V \text{ for } r \leq R}$$

for  $r \geq R$  entire  $Q$  enclosed

$$E = \frac{1}{4\pi\epsilon_0} \frac{Q}{r^2} \hat{r} \quad \vec{E} = \frac{1}{4\pi\epsilon_0} \int \frac{\rho \hat{n}}{r^2} dt' = \frac{1}{4\pi\epsilon_0} \frac{Q}{\frac{4}{3}\pi R^3} \int \frac{\hat{n}}{r^2} dt'$$

$$\frac{1}{4\pi\epsilon_0} \frac{Q}{r^2} \hat{r} = \frac{1}{4\pi\epsilon_0} \frac{Q}{\frac{4}{3}\pi R^3} \int \frac{\hat{n}}{r^2} dt'$$

$$\Rightarrow \int \frac{\hat{n}}{r^2} dt' = \frac{Q}{r^2} \hat{r} \frac{\frac{4}{3}\pi R^3}{Q} = \frac{4}{3}\pi \frac{R^3}{r^2} \hat{r}$$

$$V = \frac{\vec{P}}{4\pi\epsilon_0} \cdot \int \frac{\hat{n}}{r^2} dt' = (\vec{P} \cdot \hat{r}) \left( \frac{1}{4\pi\epsilon_0} \right) \left( \frac{4}{3}\pi \frac{R^3}{r^2} \right) = \frac{R^3}{3\epsilon_0 r^2} (\vec{P} \cdot \hat{r})$$

$$V = \frac{R^3}{3\epsilon_0 r^2} (P \cos \theta) \quad \text{for } r \geq R$$

W

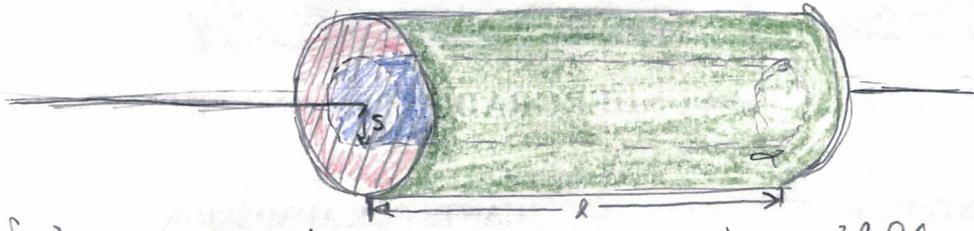
4.13

A VERY LONG CYLINDER, OF RADIUS  $a$ , CARRIES A UNIFORM POLARIZATION

$\vec{P}$  PERPENDICULAR TO ITS AXIS. FIND THE ELECTRIC FIELD INSIDE THE

CYLINDER. FIRST FIND  $\int \frac{\hat{n} \cdot \vec{P}}{r^2} d\tau$  FOR INSIDE CYLINDER TO SOLVE  $V = \frac{1}{4\pi\epsilon_0} \int \frac{\hat{n} \cdot \vec{P}}{r^2} d\tau$

IMAGINE UNIFORMLY CHARGED CYLINDER



$$\oint \vec{E} \cdot d\vec{a} = E(l\partial\pi s) = \frac{Q_{enc}}{\epsilon_0} = \frac{\pi s^2 l \rho}{\epsilon_0} \Rightarrow \vec{E} = \frac{\pi s^2 l \rho \hat{s}}{\epsilon_0 (l\partial\pi s)} = \frac{1}{4\pi\epsilon_0} \int \frac{\rho \hat{n}}{r^2} d\tau$$

$$\Rightarrow \int \frac{\hat{n}}{r} d\tau' = (4\pi\epsilon_0) \left( \frac{\pi s^2}{\epsilon_0 \partial\pi} \right) = \partial\pi \hat{s}$$

$$V = \frac{1}{4\pi\epsilon_0} \int \frac{\vec{P} \cdot \hat{n}}{r} d\tau' = \frac{\vec{P}}{4\pi\epsilon_0} \cdot \int \frac{\hat{n}}{r} d\tau' = \frac{\vec{P}}{4\pi\epsilon_0} \cdot \partial\pi \hat{s} = \frac{1}{\partial\epsilon_0} P s \cos\phi = \frac{1}{\partial\epsilon_0} P z$$

$$\vec{E} = -\nabla V = -\frac{\partial V}{\partial z} \hat{s} = \frac{-P}{\partial\epsilon_0} \hat{s} = E_{inside} \quad s \leq a$$

OUTSIDE

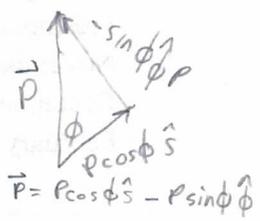


$$\oint \vec{E} \cdot d\vec{a} = E(\partial\pi s l) = \frac{Q_{enc}}{\epsilon_0} = \frac{\pi a^2 l \rho}{\epsilon_0} \Rightarrow \vec{E} = \frac{\pi a^2 l \rho \hat{s}}{\epsilon_0 (\partial\pi s l)} = \frac{1}{4\pi\epsilon_0} \int \frac{\rho \hat{n}}{r^2} d\tau'$$

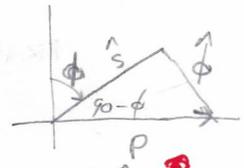
$$\Rightarrow \int \frac{\hat{n}}{r^2} d\tau' = (4\pi\epsilon_0) \left( \frac{\pi a^2 \hat{s}}{\epsilon_0 (\partial\pi s)} \right) = \frac{\partial\pi a^2 \hat{s}}{s}$$

$$V = \frac{\vec{P}}{4\pi\epsilon_0} \cdot \int \frac{\hat{n}}{r^2} d\tau' = \frac{\vec{P}}{4\pi\epsilon_0} \cdot \frac{\partial\pi a^2 \hat{s}}{s} = \frac{a^2}{\partial\epsilon_0 s} \vec{P} \cdot \hat{s} = \frac{a^2 P \cos\phi}{\partial\epsilon_0 s}$$

$$\begin{aligned} \vec{E} = -\nabla V &= -\hat{s} \frac{\partial}{\partial s} \left( \frac{a^2 P \cos\phi}{\partial\epsilon_0 s} \right) - \hat{\phi} \frac{\partial}{\partial \phi} \left( \frac{a^2 P \cos\phi}{\partial\epsilon_0 s} \right) \\ &= -\hat{s} \left( \frac{\partial P \cos\phi}{\partial\epsilon_0} \right) \left( -\frac{1}{s^2} \right) - \hat{\phi} \left( \frac{a^2 P}{\partial\epsilon_0 s^2} \right) (-\sin\phi) \\ &= \frac{P a^2 \cos\phi}{\partial\epsilon_0 s^2} \hat{s} + \frac{P a^2 \sin\phi}{\partial\epsilon_0 s} \hat{\phi} = \frac{a^2}{\partial\epsilon_0 s^2} (P \cos\phi \hat{s} + P \sin\phi \hat{\phi}) \\ &= \frac{a^2}{\partial\epsilon_0 s^2} (P \cos\phi \hat{s} + P \sin\phi \hat{\phi}) \quad \text{ok} \\ &\neq \frac{a^2}{\partial\epsilon_0 s^2} (\partial(P \cos\phi \hat{s}) - \vec{P}) \end{aligned}$$



$$E_{out} = \frac{a^2}{\partial\epsilon_0 s^2} (\partial(\vec{P} \cdot \hat{s}) \hat{s} - \vec{P})$$



10

is also right,  $m s^2$  is solution but check posted solution  $P = P \cos\phi \hat{s} - P \sin\phi \hat{\phi}$

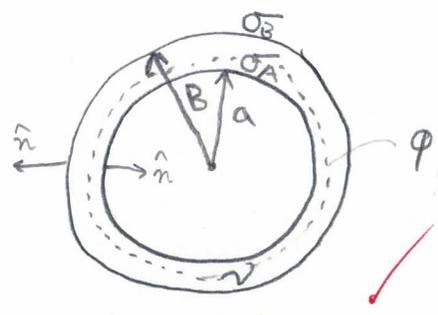
**4.15** A thick spherical shell is made of dielectric with an intrinsic polarization

$P(\vec{r}) = \frac{k}{r} \hat{r}$  where  $k$  is a constant and  $r$  is the radial distance from center. 39/40

(a) locate all bound charge and then use Gauss's LAW TO FIND  $\vec{E}$ .

$$\sigma_B = \vec{P} \cdot \hat{n} = \frac{k}{r} \hat{r} \cdot \hat{r} \Big|_{r=B} = \frac{k}{B}$$

$$\sigma_A = \vec{P} \cdot \hat{n} = \frac{k}{r} \hat{r} \cdot (-\hat{r}) \Big|_{r=a} = -\frac{k}{a}$$



$$D_{SHELL} = -\nabla \cdot \vec{P} = -\frac{1}{r^2} \frac{\partial}{\partial r} (r^2 \frac{k}{r}) = -\frac{1}{r^2} \frac{\partial}{\partial r} (kr) = -\frac{k}{r^2} \text{ for } a < r < b.$$

INSIDE SHELL

$$\epsilon_0 \oint \vec{E} \cdot d\vec{a} = \epsilon_0 E (4\pi r^2) = Q_{enc}$$

$$Q_{enc} = \int_V \rho d\tau + \sigma_A (4\pi a^2) = \int_{\phi} -\frac{k}{r^2} r^2 d\Omega - \frac{k}{a} 4\pi a^2 = -k(4\pi)(r-a) - 4\pi k a$$

$$\epsilon_0 E (4\pi r^2) = k(4\pi r + 4\pi a - 4\pi a) = -k 4\pi r \Rightarrow \boxed{\vec{E} = \frac{-k}{\epsilon_0 r} \hat{r} \quad a < r < b}$$

OUTSIDE SHELL

$$\epsilon_0 (4\pi r^2) = Q_{enc}, \quad Q_{enc} = \int_V \rho d\tau + \sigma_B (4\pi B^2) + \sigma_A (4\pi a^2)$$

$$= \int_V -k d\Omega + 4\pi k B - 4\pi k a$$

$$= (a-B)(4\pi k) + 4\pi k B - 4\pi k a$$

$$= 0 \Rightarrow \boxed{\vec{E} = \vec{0}, \quad r > b}$$

and of course  $\boxed{\vec{E} = \vec{0} \text{ for } r < a}$  as  $Q_{enc} = 0$  in that region

4.15

(b) Use Eq. 4.23 to find  $\vec{D}$  and then get  $\vec{E}$  from 4.21

$$\oint \vec{D} \cdot d\vec{a} = 4\pi r^2 D = 0 \Rightarrow \vec{D} = \vec{0}.$$

$$\vec{D} \equiv \epsilon_0 \vec{E} + \vec{P}$$

$$(i) r < a \quad \vec{P} = \vec{0} \Rightarrow \vec{0} = \epsilon_0 \vec{E} + \vec{0} \Rightarrow \vec{E} = \vec{0}$$

$$(ii) a < r < b, \quad \vec{P} = \frac{k}{r} \hat{r} \Rightarrow \vec{0} = \epsilon_0 \vec{E} + \frac{k}{r} \hat{r} \\ \Rightarrow \vec{E} = -\frac{k}{\epsilon_0 r} \hat{r}$$

$$(iii) r > b, \quad \vec{P} = \vec{0} \Rightarrow \vec{0} = \epsilon_0 \vec{E} + \vec{0} \Rightarrow \vec{E} = \vec{0}$$

$$\vec{E} = \left\{ \begin{array}{l} 0 \\ \frac{-k}{\epsilon_0 r} \hat{r} \\ 0 \end{array} \right\}_{\substack{r < a \\ a < r < b \\ r > b}} = -P/\epsilon_0$$

10

4.16 SUPPOSE THE FIELD INSIDE A DIELECTRIC IS  $\vec{E}_0$  such that  $\vec{D}_0 = \epsilon_0 \vec{E}_0 + \vec{P}$

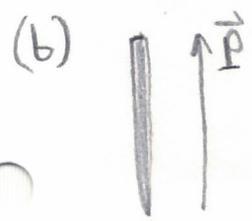
(a) a small spherical cavity is hollowed out of the material. Find the field at the center in terms of  $\vec{E}_0$  and  $\vec{P}$

from the previous work if  $\vec{P}$  points upward  
 then  $\vec{E} = -\frac{1}{3\epsilon_0} \vec{P}$  so  $\vec{E} = \frac{1}{3\epsilon_0} \vec{P}$  from Ex. 4.2.

$$\vec{E}_{net} = \vec{E}_0 + \frac{1}{3\epsilon_0} \vec{P} \quad \checkmark$$

$$\vec{D} \equiv \epsilon_0 \vec{E} + \vec{P} = \epsilon_0 \left( \vec{E}_0 + \frac{1}{3\epsilon_0} \vec{P} \right) = \epsilon_0 \vec{E}_0 + \vec{P} - \frac{2}{3} \vec{P}$$

$$\text{as } \vec{D}_0 = \epsilon_0 \vec{E}_0 + \vec{P} \Rightarrow \vec{D} = \vec{D}_0 - \frac{2}{3} \vec{P} \quad \checkmark$$



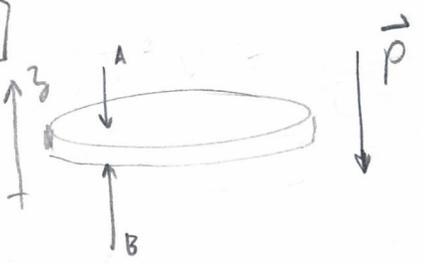
As the needle is sooooo tiny no appreciable  $\sigma$  can accumulate at either end thus the  $E$  field between them is zero.

$$\vec{E}_{net} = \vec{E}_0 + \vec{0} = \boxed{\vec{E}_0 = \vec{E}} \quad \checkmark \text{ also } \vec{P} = 0 \text{ as we removed material}$$

$$\vec{D} = \epsilon_0 \vec{E} + \vec{P} = \epsilon_0 \vec{E}_0 + \vec{P} - \vec{P} = \boxed{\vec{D}_0 - \vec{P} = \vec{D}}$$

4.16

(c)



$$\sigma_A = \vec{P} \cdot \hat{z} = -P$$

$$\sigma_B = \vec{P} \cdot (-\hat{z}) = P$$

$$\vec{E} = \frac{\sigma_A}{2\epsilon_0} \hat{z} + \frac{\sigma_B}{2\epsilon_0} (-\hat{z}) = \frac{-P}{2\epsilon_0} \hat{z} + \frac{P}{2\epsilon_0} \hat{z} = \frac{P}{\epsilon_0} \hat{z} = \frac{\vec{P}}{\epsilon_0}$$

$$\vec{E} = E_0 + \frac{\vec{P}}{\epsilon_0}$$

then  $\vec{D} = \epsilon_0 \vec{E} + \vec{P}$  as we cut it out

$$\vec{D} = \epsilon_0 \vec{E} = \epsilon_0 \left( E_0 + \frac{\vec{P}}{\epsilon_0} \right) = \vec{D}_0 = \vec{D}$$

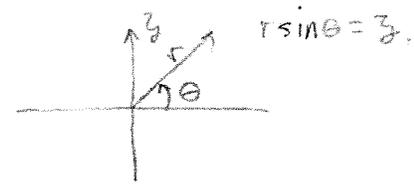


16

4.22 A very long cylinder of linear dielectric material is placed in an otherwise uniform field  $\vec{E}_0$ . Find field inside cylinder with susceptibility  $\chi_e$



$r$  = radial distance from axis



BOUNDARY CONDITIONS

- (i)  $V_{in} = V_{out}$  at  $r = a$
- (ii)  $\epsilon \frac{\partial V_{in}}{\partial r} = \epsilon_0 \frac{\partial V_{out}}{\partial r}$  at  $r = a$
- (iii)  $V_{out} \rightarrow -r \sin \theta E_0$  as  $\vec{E} = -\nabla V$  and  $-\frac{\partial(-E_0 z)}{\partial z} = E_0 = -\frac{\partial}{\partial z} E_0$

GENERAL SOLUTION for problems that possess cylindrical symmetry.

$$V(r, \theta) = a_0 + b_0 \ln(r) + \sum_{n=1}^{\infty} \{ r^n (a_n \cos(n\theta) + b_n \sin(n\theta)) + r^{-n} (c_n \cos(n\theta) + d_n \sin(n\theta)) \}$$

$$V_{in} = a_0 + \sum_{n=1}^{\infty} r^n (a_n \cos(n\theta) + b_n \sin(n\theta)) \text{ as } r^{-n}, \ln(r) \rightarrow \infty \text{ as } r \rightarrow 0.$$

$$V_{out} = -r E_0 \sin \theta + \sum_{n=1}^{\infty} r^{-n} (c_n \cos(n\theta) + d_n \sin(n\theta)) \text{ as all other terms would cause } V_{out} \neq -r E_0 \sin \theta \text{ for } r \rightarrow \infty.$$

$$\left. \frac{\partial V_{in}}{\partial r} \right|_{r=a} = \sum_{n=1}^{\infty} n a^{n-1} (a_n \cos(n\theta) + b_n \sin(n\theta))$$

$$\left. \frac{\partial V_{out}}{\partial r} \right|_{r=a} = -E_0 \sin \theta + \sum_{n=1}^{\infty} -n a^{-n-1} (c_n \cos(n\theta) + d_n \sin(n\theta))$$

$$\epsilon_0 (1 + \chi_e) \left\{ \sum_{n=1}^{\infty} n a^{n-1} (a_n \cos(n\theta) + b_n \sin(n\theta)) \right\} = \epsilon_0 \left\{ -E_0 \sin \theta + \sum_{n=1}^{\infty} -n a^{-n-1} (c_n \cos(n\theta) + d_n \sin(n\theta)) \right\}$$

the above implies that all terms with  $n \neq 1$  must be zero or else a contradiction is reached as the  $\sin \theta$  term cannot be canceled by any  $n \neq 1$  sin or cos.

$$\epsilon_0 (1 + \chi_e) [a_1 \cos \theta + b_1 \sin \theta] = \epsilon_0 [-E_0 \sin \theta - a^{-2} (c_1 \cos \theta + d_1 \sin \theta)]$$

$$V_{in} = a_0 + a_1 (a_1 \cos \theta + b_1 \sin \theta) = -r E_0 \sin \theta + a^{-1} (c_1 \cos \theta + d_1 \sin \theta)$$

$$a a_1 = a^{-1} c_1, \quad \epsilon_0 (1 + \chi_e) a_1 = \epsilon_0 (-a^{-2}) c_1$$

$$a b_1 = -r E_0 + a^{-1} d_1, \quad \epsilon_0 (1 + \chi_e) b_1 = \epsilon_0 (-E_0 - a^{-2} d_1)$$

$$a^2 = \frac{c_1}{a_1} \text{ but } a^2 = \frac{-c_1}{(1 + \chi_e) a_1} \Rightarrow a_1 = c_1 = 0.$$

$$\text{then } b_1 = \frac{-r E_0 + a^{-1} d_1}{a} \Rightarrow \epsilon_0 (1 + \chi_e) \left( \frac{-r E_0 + a^{-1} d_1}{a} \right) = \epsilon_0 (-E_0 - a^{-2} d_1)$$

$$(1 + \chi_e) \left( \frac{-r E_0}{a} \right) + E_0 = -a^{-2} d_1 - (1 + \chi_e) \frac{a^{-1}}{a} d_1 =$$

A.22

$$(1 + \chi_e) \left( \frac{-r E_0}{a} \right) + E_0 = -a^{-2} (d_1 + (1 + \chi_e) d_1)$$

(r=a)

$$(1 + \chi_e) (-E_0) + E_0 = d_1 \left( \frac{1 + 1 + \chi_e}{a^2} \right)$$

$$-E_0 - \chi_e E_0 + E_0 = d_1 \left( \frac{2 + \chi_e}{-a^2} \right)$$

$$d_1 = \frac{a^2 \chi_e E_0}{(2 + \chi_e)}$$

$$b_1 = -E_0 + \frac{d_1}{a^2} = -E_0 + \frac{\chi_e E_0}{(2 + \chi_e)}$$

$$V_{in} = a_0 + \sum_{n=1}^{\infty} r^n (a_n \cos n\theta + b_n \sin n\theta) \quad \text{0 if } n \neq 1$$

thus  $V_{in} = r \left( -E_0 + \frac{\chi_e E_0}{2 + \chi_e} \right) \sin \theta$

$\frac{-2\epsilon_0 E_0 \cos \phi}{\epsilon + \epsilon_0}$

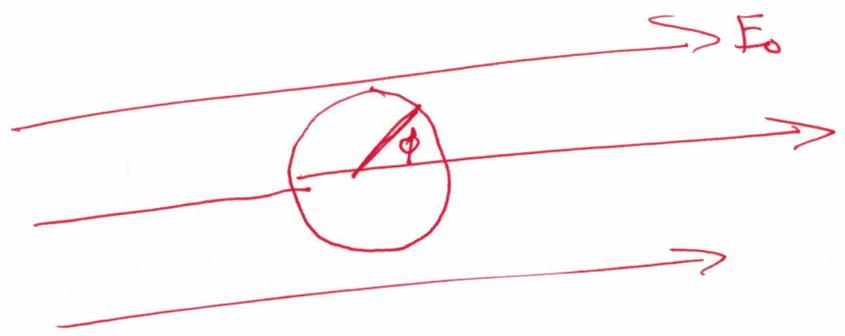
$$= r E_0 \left( \frac{-2 - \chi_e + \chi_e}{2 + \chi_e} \right) \sin \theta$$

$$V_{in} = \frac{-2 r E_0 \sin \theta}{2 + \chi_e}$$

note this would differ if one set up  $\theta$  differently.

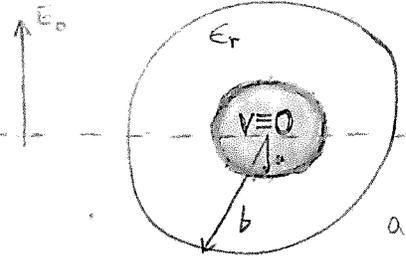
$$\vec{E} = -\nabla V = \left[ \frac{-\partial}{\partial z} \left( \frac{-2 E_0 z}{2 + \chi_e} \right) \right] \hat{z} = \frac{-2 E_0}{2 + \chi_e} \hat{z} = \frac{-2 \vec{E}_0}{2 + \chi_e} = \vec{E}_{in}$$

10



**4.24** A conducting sphere of radius  $a$ , is coated with a thick insulator (dielectric  $\epsilon_r$ ) out to radius  $b$  the object is placed in an otherwise uniform field  $\vec{E}_0$ . Find the  $\vec{E}$  field in the insulator.

$$V(r, \theta) = \sum_{l=0}^{\infty} (A_l r^l + B_l / r^{l+1}) P_l(\cos \theta)$$



Since  $V_{out} \rightarrow -E_0 r \cos \theta$  for  $r \gg R$   
 $\Rightarrow V_{out} = -E_0 r \cos \theta + \sum_{l=0}^{\infty} \frac{B_l}{r^{l+1}} P_l(\cos \theta)$

$a < r < b$   $V_{in} = \sum_{l=0}^{\infty} (A_l r^l + C_l / r^{l+1}) P_l(\cos \theta)$

$$V_{in}(a, \theta) = 0 = \sum_{l=0}^{\infty} (A_l a^l + C_l / a^{l+1}) P_l(\cos \theta) \Rightarrow A_l = -C_l / a^{2l+1}$$

$$= \sum_{l=0}^{\infty} \left( C_l \left( \frac{1}{r^{2l+1}} - \frac{r^l}{a^{2l+1}} \right) \right) P_l(\cos \theta)$$

$$\epsilon_r \frac{\partial V_{in}}{\partial r} \Big|_b = \epsilon_0 \frac{\partial V_{out}}{\partial r} \Big|_b \Rightarrow \frac{\epsilon_r}{\epsilon_0} \frac{\partial V_{in}}{\partial r} \Big|_b = \epsilon_r \frac{\partial V_{in}}{\partial r} \Big|_b = \frac{\partial V_{out}}{\partial r} \Big|_b$$

$$\frac{\partial}{\partial r} \left( \sum_{l=0}^{\infty} \left( C_l \left( \frac{1}{r^{2l+1}} - \frac{r^l}{a^{2l+1}} \right) \right) P_l(\cos \theta) \right) \Big|_b = \sum_{l=0}^{\infty} C_l P_l(\cos \theta) \left[ \frac{-l-1}{b^{2l+2}} - \frac{l b^{l-1}}{a^{2l+1}} \right] = \frac{\partial V_{in}}{\partial r} \Big|_b$$

$$\frac{\partial}{\partial r} \left( -E_0 r \cos \theta + \sum_{l=0}^{\infty} \frac{B_l}{r^{l+1}} P_l(\cos \theta) \right) \Big|_b = -E_0 \cos \theta + \sum_{l=0}^{\infty} \frac{-l-1}{b^{l+2}} P_l(\cos \theta) B_l$$

$$\epsilon_r \left( \sum_{l=0}^{\infty} C_l P_l(\cos \theta) \left[ \frac{-l-1}{b^{2l+2}} - \frac{l b^{l-1}}{a^{2l+1}} \right] \right) = -E_0 \cos \theta + \sum_{l=0}^{\infty} \frac{-l-1}{b^{l+2}} P_l(\cos \theta) B_l$$

if  $l \neq 1$  then  $0 = -E_0 \cos \theta \Rightarrow l$  must be just one for surviving terms

$$\epsilon_r C_1 \cos \theta \left[ \frac{-2}{b^3} - \frac{1}{a^3} \right] = -E_0 \cos \theta - \frac{2B_1}{b^3} \cos \theta$$

$$C_1 = \frac{-E_0 \cos \theta - \frac{2B_1}{b^3} \cos \theta}{\epsilon_r \cos \theta \left[ \frac{-2}{b^3} - \frac{1}{a^3} \right]} \Rightarrow V_{in} = \frac{-E_0 - \frac{2B_1}{b^3}}{\epsilon_r \left[ \frac{-2}{b^3} - \frac{1}{a^3} \right]} \left( \frac{1}{b^2} - \frac{b}{a^3} \right) P_1 =$$

$$V_{in}|_{r=b} = V_{out}|_{r=b}$$

$$\frac{-\epsilon_0 - \frac{\partial B_1}{b^3}}{\epsilon_r \left[ \frac{-2}{b^3} - \frac{l}{a^3} \right]} \left( \frac{1}{b^2} - \frac{b}{a^3} \right) P_1 = -E_0 b \cos \theta + \frac{B_1}{b^2} \cos \theta$$

$$-\left( \frac{1}{b^2} - \frac{b}{a^3} \right) \frac{\epsilon_0 + \epsilon_0 b}{\left( \frac{-2}{b^3} - \frac{l}{a^3} \right)} = B_1 \left( \frac{1}{b^2} + \frac{\left( \frac{1}{b^2} - \frac{b}{a^3} \right)}{\left( \frac{-2}{b^3} - \frac{l}{a^3} \right)} \right)$$

$$B_1 = \frac{Q \epsilon_0 + E_0 b}{Q} = \epsilon_0 + \frac{E_0 b}{Q}$$

$$C_1 = \frac{-\epsilon_0 - \frac{\partial B_1}{b^2}}{\epsilon_r \left[ \frac{-2}{b^3} - \frac{l}{a^3} \right]} = \frac{-\epsilon_0}{\alpha} - \frac{\partial}{\alpha b^2} \left( \epsilon_0 + \frac{E_0 b}{\left( \frac{-2}{b^3} - \frac{l}{a^3} \right)} \right)$$

$$C_1 = \frac{-\epsilon_0 - \frac{\partial}{b^2} \epsilon_0 - \partial E_0 b \left( \frac{-2/b^3 - l/a^3}{1/b^2 - b/a^3} \right)}{\epsilon_r \left[ \frac{-2}{b^3} - \frac{l}{a^3} \right]}$$

$$= \frac{-\epsilon_0 \left( 1 + \frac{\partial}{b^2} \right) - \partial E_0 b \left( \frac{-2/b^3 - l/a^3}{1/b^2 - b/a^3} \right)}{\epsilon_r \left( \frac{-2}{b^3} - \frac{l}{a^3} \right)}$$

$$= \frac{-\epsilon_0 \left( 1 + \frac{\partial}{b^2} \right) - \partial E_0 b \left( \frac{1}{1/b^2 - b/a^3} \right)}{\epsilon_r \left( \frac{-2}{b^3} - \frac{l}{a^3} \right) \left( \frac{1}{b^2} - \frac{b}{a^3} \right)}$$

$l=1$ .

$$= \left( \frac{1}{b^2} - \frac{b}{a^3} + \frac{2}{b^4} - \frac{\partial}{ab} \right) (-\epsilon_0) - \partial E_0 \epsilon_r \left( \frac{-2}{b^2} - \frac{b}{a^3} \right) =$$

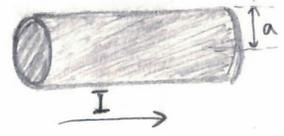
$$E_{in} = -\nabla V_{in} = \frac{\partial}{\partial r} \left( C_1 \left( \frac{1}{r^2} - \frac{r}{a^3} \right) \cos \theta \right) \hat{r} - \frac{\partial}{\partial \theta} \left( C_1 \left( \frac{1}{r^2} - \frac{r}{a^3} \right) \cos \theta \right) \hat{\theta} = \boxed{C_1 \left( \frac{2}{r^3} + \frac{3}{a^3} \right) \cos \theta \hat{r} - \left( \frac{1}{r^2} - \frac{r}{a^3} \right) \sin \theta \hat{\theta}}$$

where  $C_1 = \frac{-\epsilon_0 \left( 1 + \frac{\partial}{b^2} \right) - \partial E_0 \left( \frac{-2/b^2 - b/a^3}{1/b^2 - b/a^3} \right)}{\epsilon_r \left[ \frac{-2}{b^3} - \frac{1}{a^3} \right]}$  ↑ Check this ↑ almost just could get  $C_1$  to work out.

5.13

$s \equiv r$

(a)

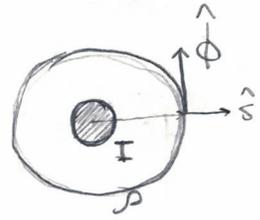


$$\oint \vec{B} \cdot d\vec{l} = \mu_0 I_{enc}$$

$I_{enc}$  for  $r < a$  is zero  $\Rightarrow \vec{B} = 0$

$I_{enc}$  for  $r > a$  is  $I$  thus  $\oint \vec{B} \cdot d\vec{l} = \mu_0 I = B(2\pi r) \Rightarrow \vec{B} = \frac{\mu_0 I}{2\pi r}$

$$B = \begin{cases} 0 & \text{for } r < a \\ \frac{\mu_0 I}{2\pi r} & \text{for } r > a \end{cases} \text{ which is in } \hat{\phi} \text{ direction}$$



18/20

(b) The current density  $J$  is proportional to  $r$ , where  $r$  is the distance from axis

$$J = \frac{dI}{da_{\perp}} = kr \Rightarrow dI = kr da_{\perp} = kr(2\pi r dr)$$

$$\int dI = I_{enc} = \int_0^r 2\pi k r^2 dr = \frac{2\pi k r^3}{3} = I$$

$$I_{enc}(a) \Rightarrow k = \frac{3I}{2\pi a^3}$$

$$\Rightarrow I_{enc} = \frac{2\pi}{3} \left( \frac{3I}{2\pi a^3} \right) r^3$$

$$\Rightarrow I_{enc} = \frac{I}{a^3} r^3$$



$$\oint \vec{B} \cdot d\vec{l} = \mu_0 I_{enc} = (2\pi r) B_{in} = \mu_0 \left( \frac{I}{a^3} r^3 \right)$$

$$B_{in} = \frac{\mu_0 I}{2\pi a^3} r^2$$

$$B = \begin{cases} \frac{\mu_0 I}{2\pi a^3} r^2 & \text{if } r < a \\ \frac{\mu_0 I}{2\pi r} & \text{if } r > a \end{cases} \text{ again in the } \hat{\phi} \text{ direction}$$

10

5.19

(a) find  $\rho$  for electrons in copper wire, assume 2 free  $e^-$  for atoms.  
 $D = \text{density of copper} = 8900 \text{ kg/m}^3 = 8.9 \times 10^6 \text{ g/m}^3$

63.59 g/mol of copper

$$\rho = \left(8.9 \times 10^6 \frac{\text{g}}{\text{m}^3}\right) \left(\frac{1}{63.59 \frac{\text{g}}{\text{mol}}}\right) \left(6.023 \times 10^{23} \frac{\text{atoms}}{\text{mol}}\right) \left(\frac{2e^-}{\text{atom}}\right) = 1.686 \times 10^{29} \frac{e^-}{\text{m}^3} = \rho$$

$$= 2.7 \times 10^{10} \frac{\text{C}}{\text{m}^3} = \rho$$

(b)  $J = \frac{dI}{da_{\perp}} = \rho v$

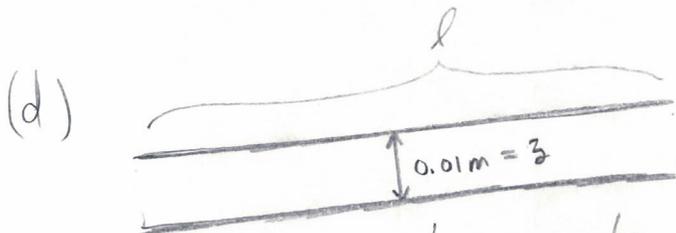
$$v = \frac{dI}{\rho da_{\perp}} = \frac{I}{\rho a} = \frac{I}{\rho (\pi (\frac{d}{2})^2)} = \frac{(1 \text{ C/s}) 4}{(2.7 \times 10^{10} \frac{\text{C}}{\text{m}^3}) \pi (0.001 \text{ m})^2} = 4.716 \times 10^{-5} \frac{\text{m}}{\text{s}}$$

(c) The force of attraction must depend on the length of the wire involved thus the  $F$  will be in terms of then length of wire.  $l = \text{length}$

$\vec{F} = i \vec{l} \times \vec{B}$  where  $B = \frac{\mu_0 I}{2\pi r}$  where  $r = 0.01 \text{ m}$   
 $I = 1 \text{ A}$   
 $\mu_0 = 4\pi \times 10^{-7} \text{ N/A}^2$

$$F = i l B = (1 \text{ A}) l \left(\frac{4\pi \times 10^{-7} \text{ N/A}^2}{2\pi (0.01 \text{ m})}\right) (1 \text{ A}) = l (2 \frac{\text{N}}{\text{m}} \times 10^{-5}) = F_B$$

if  $l = 1 \text{ m}$  then  $F_B = (2 \times 10^{-5}) \text{ N}$



$$\rho = \frac{Q}{V} = \frac{Q}{lA}$$

$Q = \rho l a$  by symmetry  
 $F = \frac{1}{4\pi\epsilon_0} \frac{Q Q}{r^2}$

8  $F = \frac{1}{4\pi\epsilon_0} \frac{\rho^2 l^2 a^2}{r^2} = l^2 \left(\frac{(2.7 \times 10^{10})^2 (\pi (0.0005)^2)^2}{0.0001} \frac{\text{N}}{\text{m}^2}\right) = l^2 (4.043 \times 10^{22} \frac{\text{N}}{\text{m}^2}) = F_E$

$F_E = \alpha F_B \Rightarrow \alpha = \frac{F_E}{F_B} = \frac{l^2 (4.043 \times 10^{22} \frac{\text{N}}{\text{m}^2})}{l (2 \frac{\text{N}}{\text{m}} \times 10^{-5})} = l (2.021 \times 10^{27})$

This question is poor. Assume  $l = 1 \text{ m}$

then  $F_E = (2.021 \times 10^{27}) F_B$

this many times greater.  
 see soln

5.24 If  $\vec{B}$  is uniform show that  $\vec{A}(\vec{r}) = -\frac{1}{2}(\vec{r} \times \vec{B})$

$$\nabla \cdot \vec{A} = \nabla \cdot \left( -\frac{1}{2} \vec{r} \times \vec{B} \right) = -\frac{1}{2} \left\{ \vec{B} \cdot (\nabla \times \vec{r}) - \vec{r} \cdot (\nabla \times \vec{B}) \right\}$$

$$\begin{aligned} \nabla \times \vec{r} &= \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ x & y & z \end{vmatrix} = \hat{i} \begin{vmatrix} \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ y & z \end{vmatrix} - \hat{j} \begin{vmatrix} \frac{\partial}{\partial x} & \frac{\partial}{\partial z} \\ x & z \end{vmatrix} + \hat{k} \begin{vmatrix} \frac{\partial}{\partial x} & \frac{\partial}{\partial y} \\ x & y \end{vmatrix} \\ &= \hat{i} \left( \frac{\partial z}{\partial y} - \frac{\partial y}{\partial z} \right) - \hat{j} \left( \frac{\partial z}{\partial x} - \frac{\partial x}{\partial z} \right) + \hat{k} \left( \frac{\partial y}{\partial x} - \frac{\partial x}{\partial y} \right) = 0 \end{aligned}$$

$$\begin{aligned} \nabla \times \vec{B} &= \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ B_x & B_y & B_z \end{vmatrix} = \hat{i} \left( \frac{\partial B_z}{\partial y} - \frac{\partial B_y}{\partial z} \right) - \hat{j} \left( \frac{\partial B_z}{\partial x} - \frac{\partial B_x}{\partial z} \right) + \hat{k} \left( \frac{\partial B_y}{\partial x} - \frac{\partial B_x}{\partial y} \right) \\ &= 0 \text{ as } B_x, B_y, B_z \text{ are just constants for a uniform } \vec{B} \text{ field.} \end{aligned}$$

thus

$$\nabla \cdot \vec{A} = -\frac{1}{2} \left\{ (\vec{B} \cdot \vec{0}) - (\vec{r} \cdot \vec{0}) \right\} = 0.$$

$$\nabla \times \vec{A} = \nabla \times \left( -\frac{1}{2} \vec{r} \times \vec{B} \right) = -\frac{1}{2} \left\{ (\vec{B} \cdot \nabla) \vec{r} - (\vec{r} \cdot \nabla) \vec{B} + \vec{r} (\nabla \cdot \vec{B}) - \vec{B} (\nabla \cdot \vec{r}) \right\}$$

$$(\vec{B} \cdot \nabla) \vec{r} = \left( B_x \frac{\partial}{\partial x} + B_y \frac{\partial}{\partial y} + B_z \frac{\partial}{\partial z} \right) (x\hat{i} + y\hat{j} + z\hat{k}) = B_x \hat{i} + B_y \hat{j} + B_z \hat{k} = \vec{B}$$

$$\vec{r} (\nabla \cdot \vec{B}) = \vec{r} \left( \frac{\partial B_x}{\partial x} + \frac{\partial B_y}{\partial y} + \frac{\partial B_z}{\partial z} \right) = 0 \text{ as } B_x, B_y, B_z \text{ are constants.}$$

$$(\vec{r} \cdot \nabla) \vec{B} = \left( x \frac{\partial}{\partial x} + y \frac{\partial}{\partial y} + z \frac{\partial}{\partial z} \right) (B_x \hat{i} + B_y \hat{j} + B_z \hat{k}) = 0 \text{ as } B_x, B_y, B_z \text{ are constant.}$$

$$\vec{B} (\nabla \cdot \vec{r}) = (B_x \hat{i} + B_y \hat{j} + B_z \hat{k}) \left( \frac{\partial x}{\partial x} + \frac{\partial y}{\partial y} + \frac{\partial z}{\partial z} \right) = 3 \vec{B}$$

$$\text{thus } \nabla \times \vec{A} = -\frac{1}{2} \left\{ \vec{B} - 3 \vec{B} \right\} = -\frac{1}{2} \left\{ -2 \vec{B} \right\} = \vec{B} \checkmark$$

there are other functions for instance let  $\vec{A}' \equiv -\frac{1}{2}(\vec{r} \times \vec{B}) + \vec{C} = \vec{A} + \vec{C}$ . where  $\vec{C}$  is a vector composed of constants. (no coordinate dependence)

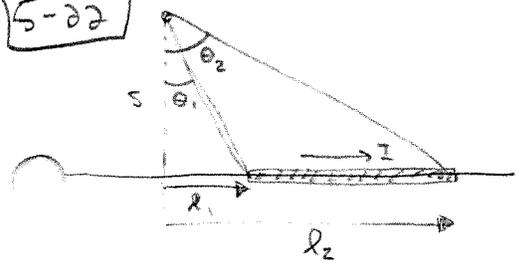
$$\text{then } \nabla \cdot \vec{A}' = \nabla \cdot \left( -\frac{1}{2} \vec{r} \times \vec{B} + \vec{C} \right) = \nabla \cdot \left( -\frac{1}{2} \vec{r} \times \vec{B} \right) + \nabla \cdot \vec{C} \text{ where } \nabla \cdot \vec{C} = 0$$

trivially and  $\nabla \cdot \left( -\frac{1}{2} \vec{r} \times \vec{B} \right) = 0$  as shown above. furthermore

$$\nabla \times \vec{A}' = \nabla \times (\vec{A} + \vec{C}) = \nabla \times \vec{A} + \nabla \times \vec{C} \text{ again } \nabla \times \vec{C} = 0 \text{ and}$$

$\nabla \times \vec{A} = \vec{B}$  as shown above. There are many vector potentials that satisfy  $\vec{B}$  being uniform.

5-22



$$l' = s \tan \theta$$

$$d\theta = \frac{s d\theta}{\cos^2 \theta}$$

$$\cos \theta = \frac{s}{\sqrt{s^2 + z_1'^2}}$$

$$\theta = \tan^{-1}\left(\frac{l'}{s}\right)$$

$$\frac{1}{r} = \frac{\cos \theta}{s}$$

$$\vec{A} = \frac{\mu_0}{4\pi} \int \frac{I d\vec{l}'}{r} = \frac{\mu_0 I}{4\pi} \int \frac{dl'}{r} = \frac{\mu_0 I}{4\pi} \int \frac{s d\theta}{\cos^2 \theta} \frac{\cos \theta}{s} = \frac{\mu_0 I}{4\pi} \int_{\theta_1}^{\theta_2} \frac{d\theta}{\cos \theta}$$

$$= \frac{\mu_0 I}{4\pi} \ln \left\{ \tan\left(\frac{\pi}{4} + \frac{\theta}{2}\right) \right\} \Big|_{\theta_1}^{\theta_2} = \frac{\mu_0 I}{4\pi} \left\{ \ln\left(\tan\left(\frac{\pi}{4} + \frac{\theta_2}{2}\right)\right) - \ln\left(\tan\left(\frac{\pi}{4} + \frac{\theta_1}{2}\right)\right) \right\}$$

as  $\theta_1 = \tan^{-1}\left(\frac{z_1'}{s}\right)$   
 $\theta_2 = \tan^{-1}\left(\frac{z_2'}{s}\right)$

$$= \frac{\mu_0 I}{4\pi} \left\{ \ln \left[ \tan\left(\frac{\pi}{4} + \tan^{-1}\left(\frac{z_2'}{s}\right)\right) \right] - \ln \left[ \tan\left(\frac{\pi}{4} + \tan^{-1}\left(\frac{z_1'}{s}\right)\right) \right] \right\}$$

$$\nabla \times \vec{A} = -\frac{\partial V_z}{\partial s} \hat{\phi} = \hat{\phi} \frac{\mu_0 I}{4\pi} \frac{\partial}{\partial s} \left\{ \ln \left[ \tan\left(\frac{\pi}{4} + \frac{1}{2} \tan^{-1}\left(\frac{z_2'}{s}\right)\right) \right] - \ln \left[ \tan\left(\frac{\pi}{4} + \frac{1}{2} \tan^{-1}\left(\frac{z_1'}{s}\right)\right) \right] \right\}$$

$$= \hat{\phi} \frac{\mu_0 I}{4\pi} \left\{ \frac{\sec^2\left(\frac{\pi}{4} + \frac{1}{2} \tan^{-1}\left(\frac{z_2'}{s}\right)\right)}{\tan\left(\frac{\pi}{4} + \frac{1}{2} \tan^{-1}\left(\frac{z_2'}{s}\right)\right)} \frac{1/2}{(1 + (z_2'/s)^2)} \frac{-z_2'}{s^2} - \frac{\sec^2\left(\frac{\pi}{4} + \frac{\theta}{2}\right) (1/2) (-z_1')}{\tan\left(\frac{\pi}{4} + \frac{\theta}{2}\right) (1 + (z_1'/s)^2) s^2} \right\}$$

$$= \hat{\phi} \frac{\mu_0 I}{4\pi} \left\{ \frac{1}{\sin \beta_1 \cos \beta_1} \left( \frac{1/2}{1 + (z_2'/s)^2} \right) \left( \frac{-z_2'}{s^2} \right) - \frac{1}{\sin \beta_2 \cos \beta_2} \left( \frac{1/2}{1 + (z_1'/s)^2} \right) \left( \frac{-z_1'}{s^2} \right) \right\}$$

$$= \hat{\phi} \frac{\mu_0 I}{4\pi} \left\{ \frac{1}{\sin 2\beta_1} \frac{-z_2'}{s^2 + z_2'^2} - \frac{1}{\sin 2\beta_2} \frac{-z_1'}{s^2 + z_1'^2} \right\}$$

$$= \hat{\phi} \frac{\mu_0 I}{4\pi} \left\{ \frac{1}{\sin\left(\frac{2\pi}{4} + \theta_2\right)} \frac{z_2'}{s^2 + z_2'^2} - \frac{1}{\sin\left(\frac{2\pi}{4} + \theta_1\right)} \frac{z_1'}{s^2 + z_1'^2} \right\}$$

$$= \hat{\phi} \frac{\mu_0 I}{4\pi} \left\{ \frac{1}{\cos(\theta_2)} \frac{z_2'}{s^2 + z_2'^2} - \frac{1}{\cos \theta_1} \frac{z_1'}{s^2 + z_1'^2} \right\}$$

$$= \hat{\phi} \frac{\mu_0 I}{4\pi} \left\{ \frac{\sqrt{s^2 + z_2'^2}}{s} \frac{z_2'}{s^2 + z_2'^2} - \frac{\sqrt{s^2 + z_1'^2}}{s} \frac{z_1'}{s^2 + z_1'^2} \right\}$$

$$= \hat{\phi} \frac{\mu_0 I}{4\pi} \left\{ \frac{z_2'}{\sqrt{s^2 + z_2'^2}} \frac{1}{s} - \frac{z_1'}{\sqrt{s^2 + z_1'^2}} \frac{1}{s} \right\}$$

$$= \hat{\phi} \frac{\mu_0 I}{4\pi s} \left\{ \sin \theta_2 - \sin \theta_1 \right\} \text{ happy day.}$$

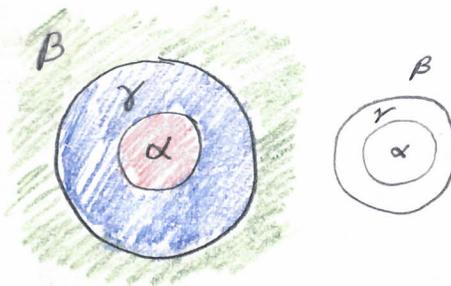
4-26 A spherical conductor of radius  $a$ , carries a charge  $Q$ . It's surrounded by linear dielectric material of  $\chi_e$  out to radius  $b$ . find the energy of this configuration.

$$\oint \vec{D} \cdot d\vec{a} = Q_{enc} = Q \quad \text{for } r > a \quad \vec{D} = \frac{Q}{4\pi r^2} \hat{r}$$

$$\vec{D} = 0 \quad \text{for } r < a$$

20/20

$$\vec{E} = \begin{cases} \frac{Q}{4\pi\epsilon r^2} \hat{r} & a < r < b \\ \frac{Q}{4\pi\epsilon_0 r^2} \hat{r} & r > b \\ 0 & r < a \end{cases}$$



$$W = \frac{1}{2} \int_{\text{all space}} \vec{D} \cdot \vec{E} \, d\tau = \frac{1}{2} \int_{\alpha} \vec{D} \, d\tau + \frac{1}{2} \int_{\gamma} \frac{Q \hat{r}}{4\pi r^2} \cdot \frac{Q \hat{r}}{4\pi \epsilon r^2} \, d\tau + \frac{1}{2} \int_{\beta} \frac{Q \hat{r}}{4\pi r^2} \cdot \frac{Q \hat{r}}{4\pi \epsilon_0 r^2} \, d\tau$$

$$= \frac{1}{2} \int_a^b \frac{Q^2}{(4\pi)^2 \epsilon} \frac{r^2 dr d\Omega}{r^4} + \frac{1}{2} \int_b^{\infty} \frac{Q^2}{(4\pi)^2 \epsilon_0} \frac{r^2 dr d\Omega}{r^4} = \frac{Q^2}{2(4\pi)^2 \epsilon} \int_a^b \frac{dr}{r^2} \int d\Omega + \frac{Q^2}{2(4\pi)^2 \epsilon_0} \int_b^{\infty} \frac{dr}{r^2} \int d\Omega$$

$$= \frac{Q^2}{2(4\pi)^2 \epsilon} \left( -\frac{1}{r} \Big|_a^b \right) (4\pi) + \frac{Q^2}{2(4\pi)^2 \epsilon_0} \left( -\frac{1}{r} \Big|_b^{\infty} \right) (4\pi)$$

$$= \frac{Q^2}{8\pi\epsilon} \left( \frac{1}{a} - \frac{1}{b} \right) + \frac{Q^2}{8\pi\epsilon_0} \left( \frac{1}{b} \right) = W$$

and  $\epsilon = \epsilon_0(1 + \chi_e)$

so 
$$W = \frac{Q^2}{\epsilon_0(1 + \chi_e) 8\pi} \left( \frac{1}{a} - \frac{1}{b} \right) + \frac{Q^2}{8\pi\epsilon_0} \left( \frac{1}{b} \right)$$

$$W = \frac{Q^2}{8\pi\epsilon_0} \left( \frac{1}{1 + \chi_e} \left( \frac{1}{a} - \frac{1}{b} \right) + \frac{1}{b} \right)$$

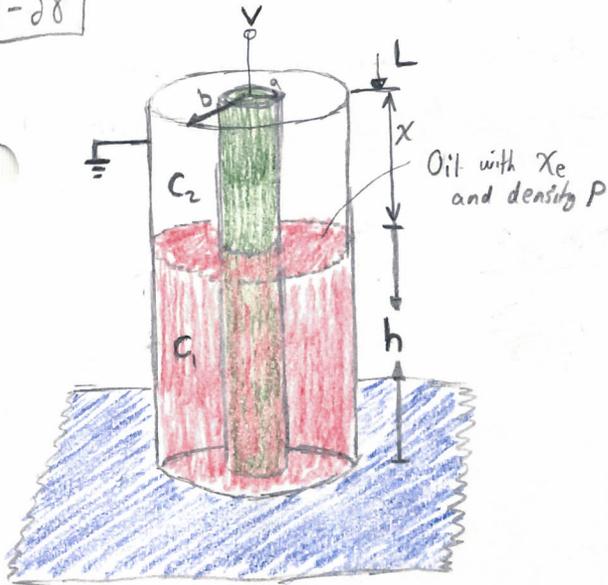
$$= \frac{Q^2}{8\pi\epsilon_0} \left( \frac{\frac{b}{a} - \frac{b}{b} + 1 + \chi_e}{b(1 + \chi_e)} \right) = \frac{Q^2}{8\pi\epsilon_0} \left( \frac{\frac{b}{a} + \chi_e}{b(1 + \chi_e)} \right) = W$$

$$W = \frac{Q^2}{8\pi\epsilon_0} \left( \frac{1}{a(1 + \chi_e)} + \frac{\chi_e}{b(1 + \chi_e)} \right)$$

$$W = \frac{Q^2}{2(4\pi\epsilon_0)} \left( \frac{b + a\chi_e}{ab(1 + \chi_e)} \right)$$

10

4-28



To what point does the oil rise in the tube?  
The oil rises as far as is energetically favorable.

THE CAPACITANCE OF THIS CYLINDER IS NOT JUST  $\frac{\epsilon A}{d}$  as before with the flat plate cap. instead it is known from work in "208" that

$$C_i = \frac{2\pi}{\ln(b/a)} \epsilon_i l_i \quad \text{where } l \text{ is the length of the cylinder}$$

$$\text{thus } C = C_1 + C_2 = \frac{2\pi}{\ln(b/a)} (\epsilon(L-x) + \epsilon_0 x) = \frac{2\pi}{\ln(b/a)} [\epsilon_0(1+\chi_e)[L-x] + \epsilon_0 \chi_e x]$$

$$\frac{dC}{dx} = \frac{2\pi}{\ln(b/a)} [-\epsilon_0(1+\chi_e) + \epsilon_0] = \frac{-2\pi \epsilon_0 \chi_e}{\ln(b/a)}$$

$$\left. \begin{array}{l} \uparrow \vec{F} \text{ (decreasing } x) \\ \downarrow mg \text{ (increasing } x) \end{array} \right\} F + mg = 0.$$

$$F = \frac{1}{2} V^2 \frac{dC}{dx} = \frac{-V^2 \pi \epsilon_0 \chi_e}{\ln(b/a)} = -mg = -\rho \pi (b^2 - a^2) h g$$

$$\Rightarrow h = \frac{V^2 \chi_e \epsilon_0}{\ln(b/a) \rho (b^2 - a^2) g}$$

10