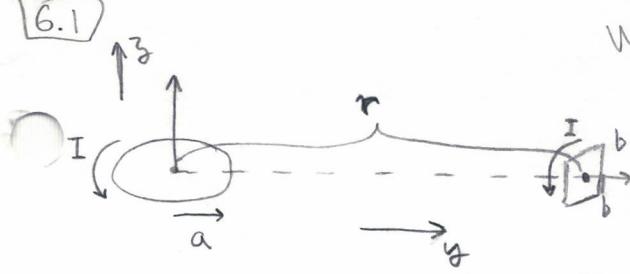


6.1



What is the torque on the square loop due to the circular one.

$$\vec{m}_1 = \pi a^2 I \hat{z}$$

20/20.

good

$$\begin{aligned}\vec{B} &= \frac{\mu_0}{4\pi r^3} \left\{ 3(\vec{m}_1 \cdot \hat{r}) \hat{r} - \vec{m}_1 \right\} = \\ &= \frac{\mu_0}{4\pi r^3} \left\{ 3(\vec{a}) \hat{r} - \vec{m}_1 \right\} \\ &= -\frac{\mu_0}{4\pi r^3} (\pi a^2 I \hat{z})\end{aligned}$$

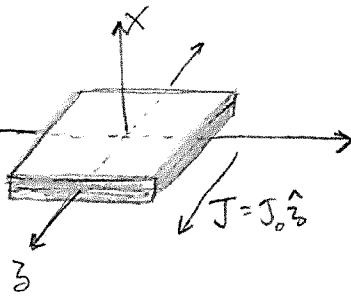
$$\vec{m}_2 = -b^2 I \hat{y}$$

$$\vec{N} = \vec{m}_2 \times \vec{B} = (b^2 I \hat{y}) \times \left(-\frac{\mu_0}{4\pi r^3} \pi a^2 I \hat{z} \right)$$

$$\begin{aligned}\vec{N} &= \frac{-b^2 I \mu_0 a^2 I \hat{x}}{4r^3} \\ &= \boxed{-\frac{a^2 b^2 I^2 \mu_0}{4r^3} \hat{x}} = \vec{N}\end{aligned}$$

The equilibrium point where $\vec{N} = 0$ is where the loop lies $x-y$ plane and m_2 is in the $\pm \hat{z}$ direction where \vec{B} is \perp to m_2 .

6.5



\vec{B} must depend only on x as a y dependence is prohibited by the symmetry of the infinite plane. No z dependence is possible by the Biot-Savart law as the cross product of \hat{z} with \hat{z} is zero. The Biot-Savart law also dictates that \vec{B} is in the \hat{z} direction.

$$\int \vec{B} \cdot d\vec{l} = \mu_0 I_{enc} = \int \mu_0 \vec{J} \cdot d\vec{a} = \mu_0 J_0 \int dx dy = \mu_0 J_0 x y = \int B dy = By$$

$$\Rightarrow \vec{B} = \mu_0 J_0 x \hat{y}$$

(a) $\vec{F} = \nabla(\vec{m} \cdot \vec{B}) = \nabla(m_0 \hat{x} \cdot \mu_0 J_0 x \hat{y}) = \nabla(0) = \boxed{\vec{0}} = \vec{F}$

(b) $\vec{F} = \nabla(\vec{m} \cdot \vec{B}) = \nabla(m_0 \hat{y} \cdot \mu_0 J_0 x \hat{y}) = \nabla(m_0 \mu_0 J_0 x)$ ✓

$$\boxed{\vec{F} = m_0 \mu_0 J_0 x \hat{x}}$$

(i)

Prove $\nabla(\vec{p} \cdot \vec{E}) = (\vec{p} \cdot \nabla) \vec{E}$ ✓

By product rule 4 we may expand $\nabla(\vec{p} \cdot \vec{E})$ to

$$\nabla(\vec{p} \cdot \vec{E}) = \vec{p} \times (\nabla \times \vec{E}) + \vec{E} \times (\nabla \times \vec{p}) + (\vec{p} \cdot \nabla) \vec{E} + (\vec{E} \cdot \nabla) \vec{p}$$

$\nabla \times \vec{E} = 0$ in electrostatics and $\nabla \times \vec{p} = 0$ as \vec{p} is just a constant vector.

$$\text{so } \nabla(\vec{p} \cdot \vec{E}) = \vec{p} \times \vec{0} + \vec{E} \times \vec{0} + (\vec{p} \cdot \nabla) \vec{E} + (\vec{E} \cdot \nabla) \vec{p} = (\vec{p} \cdot \nabla) \vec{E} + (\vec{E} \cdot \nabla) \vec{p}$$

$E \cdot \nabla = E_x \frac{\partial}{\partial x} + E_y \frac{\partial}{\partial y} + E_z \frac{\partial}{\partial z}$ and when this operator acts on \vec{p} a constant vector all the derivatives are zero

$$\Rightarrow (\vec{E} \cdot \nabla) \vec{p} = 0 \text{ thus } \nabla(\vec{p} \cdot \vec{E}) = (\vec{p} \cdot \nabla) \vec{E} + \vec{0} = \boxed{(\vec{p} \cdot \nabla) \vec{E} = \nabla(\vec{p} \cdot \vec{E})}$$

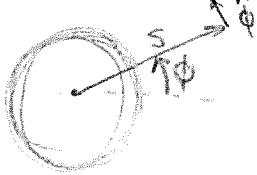
(ii)

Why does $\nabla(\vec{m} \cdot \vec{B}) \neq (m \cdot \nabla) \vec{B}$, mathematically this does not hold because $\nabla \times \vec{B} \neq 0$ in general, the other two terms vanish because \vec{m} is also just a constant vector

(iii) Calculate $(m \cdot \nabla) \vec{B}$ for (a) and (b)

$$(m_0 \hat{x} \cdot \nabla) \vec{B} = m_0 \frac{\partial}{\partial x} \vec{B} = m_0 \frac{\partial}{\partial x} (\mu_0 J_0 x \hat{y}) = m_0 \mu_0 J_0 \hat{y} \neq \vec{0} \quad \checkmark$$

$$(m_0 \hat{y} \cdot \nabla) \vec{B} = m_0 \frac{\partial}{\partial y} (\vec{B}) = m_0 \frac{\partial}{\partial y} (\mu_0 J_0 x \hat{y}) = \vec{0} \neq m_0 \mu_0 J_0 \hat{x} \quad \checkmark$$

6.8 Find \vec{B} from \vec{M} 

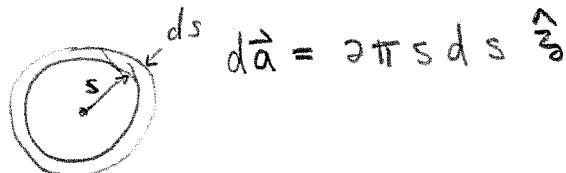
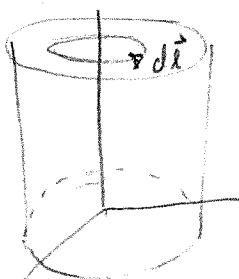
$$\vec{M} = ks^2 \hat{\phi}$$

$$\nabla \phi = ks^2, \nabla_s = 0, \nabla_\phi = 0$$

$$\begin{aligned}\vec{J}_b &= \nabla \times \vec{M} \\ &= \left[\frac{1}{s} \frac{\partial V_\phi}{\partial \phi} - \frac{\partial V_\phi}{\partial s} \right] \hat{s} + \frac{1}{s} \left[\frac{\partial}{\partial s} (s V_\phi) - \frac{\partial V_\phi}{\partial \phi} \right] \hat{\phi} \\ &= \frac{1}{s} \frac{\partial}{\partial s} (s k s^2) \hat{\phi} = \frac{1}{s} k 3 s^2 \hat{\phi} = \boxed{3 k s^3 \hat{\phi}} = \frac{\vec{M}}{s}\end{aligned}$$

$$\begin{aligned}\vec{K}_G &= \vec{M} \times \hat{n} \\ &= k s^2 \hat{\phi} \times \hat{s} \\ &= -k s^2 \hat{s} \Big|_{s=R} = \boxed{-k R^2 \hat{s} = \vec{K}_G}\end{aligned}$$

Amperes law is appropriate if we consider the following loop

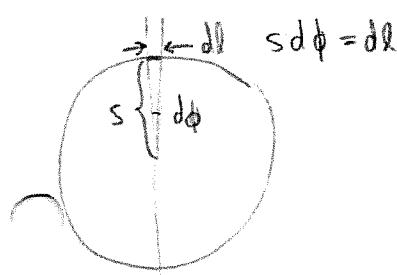
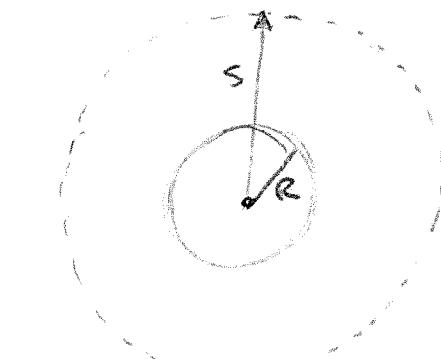


$$\begin{aligned}\oint \vec{B} \cdot d\vec{l} &= B(2\pi s) = N_0 I_{enc} = N_0 \int \vec{J} \cdot d\vec{a} \\ &= N_0 \int 3k s^3 \hat{\phi} \cdot 2\pi s ds \hat{\phi} \\ &= N_0 \int 6\pi k s^2 ds\end{aligned}$$

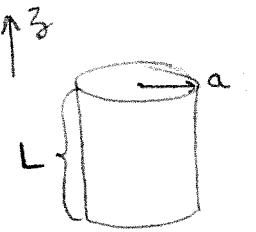
$$\begin{aligned}B(2\pi s) &= 2N_0 \pi k s^3 \\ \vec{B}_{in} &= N_0 k s^2 \hat{\phi}\end{aligned}$$

$$\begin{aligned}I_{enc} &= \int_0^R \vec{J} \cdot d\vec{a} + \int_{s=R}^{2\pi} -k R^2 s d\phi = 2\pi k s^3 \Big|_0^R + -2\pi R^2 R k \\ &= 2\pi k R^3 - 2\pi k R^3 \\ &= 0\end{aligned}$$

$$\Rightarrow \boxed{\vec{B}_{out} = \vec{0}}$$



6.9



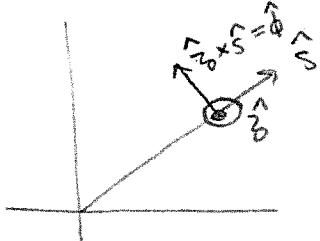
$$\vec{M} = M \hat{z} \quad \text{where } M \in \mathbb{R}$$

$$\vec{J}_B = \nabla \times \vec{M} = 0 \quad \text{as } M \text{ is constant.}$$

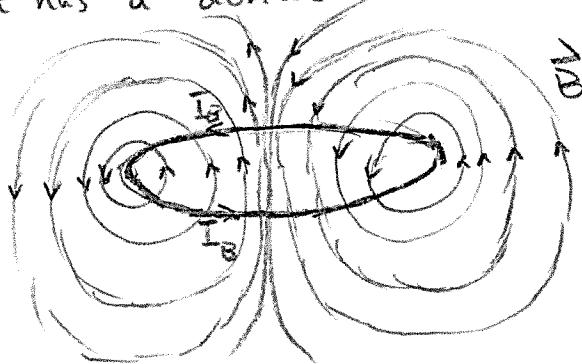
$$\vec{K}_B = \vec{M} \times \hat{n} = \vec{M} \times \hat{z} = M \hat{z} = \vec{K}_B$$

Bound Current

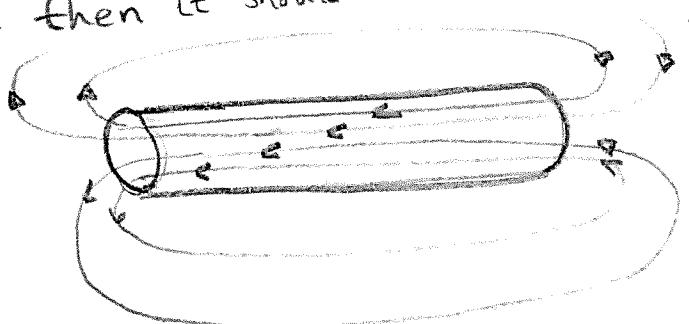
✓



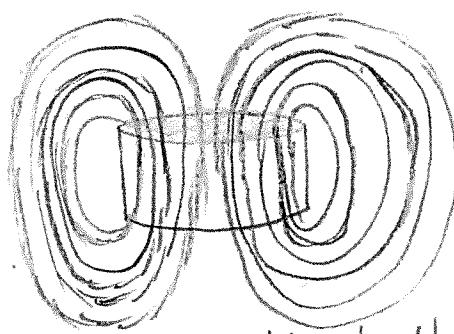
$L \ll a$ then it is just like a wire in the limit
so it has a donut like field



$L \gg a$ then it should resemble a solenoid.



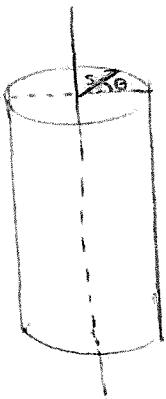
for an ideal
solenoid $\vec{B} = 0$
outside I assumed
less than perfection

 $L \approx a$ 

a compromise
between the 2
extremes of
 $a \ll L$ and $L \gg a$

from the problem 4.11 I would note this is the magnetic
analogue to the bar electret.

6.12

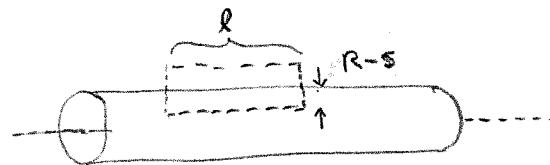
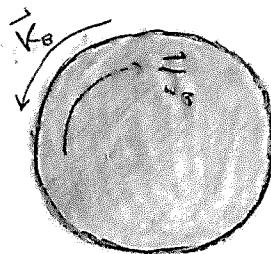


$$\vec{M} = ks \hat{z} \quad \text{where } k \text{ is a constant.}$$

20/20 good

$$(a) \vec{K}_s = \vec{M} \times \hat{n} = ks(\hat{z} \times \hat{s}) = ks\hat{\theta} = kR\hat{\theta} \quad \checkmark$$

$$\vec{J}_s = \nabla \times \vec{M} = \frac{1}{s} \frac{\partial M_3}{\partial \theta} \hat{s} - \frac{\partial M_2}{\partial s} \hat{\theta} = \frac{1}{s} \frac{\partial}{\partial \theta} (ks) \hat{s} - \frac{2}{ss} (ks) \hat{\theta} = -k \hat{\theta}$$



$$\oint \vec{B} \cdot d\vec{l} = \mu_0 I_{\text{enc}} = \mu_0 (-k(R-s)\lambda) + \mu_0 kR = B\lambda$$

$$\Rightarrow \vec{B} = \mu_0 sk - \mu_0 kR + \mu_0 kR$$

$$\boxed{\vec{B}_{\text{in}} = \mu_0 sk \hat{z}} \quad \checkmark$$



Both outside loops $\Rightarrow B$ is constant.

As B comes from a finite current distribution B_{out} must be zero

$$\boxed{\vec{B}_{\text{out}} = \vec{0}} \quad \checkmark$$

$$(b) \oint \vec{H} \cdot d\vec{l} = I_{\text{enc}} \quad \text{where} \quad \vec{H} = \frac{1}{\mu_0} (\vec{B} - \vec{M})$$

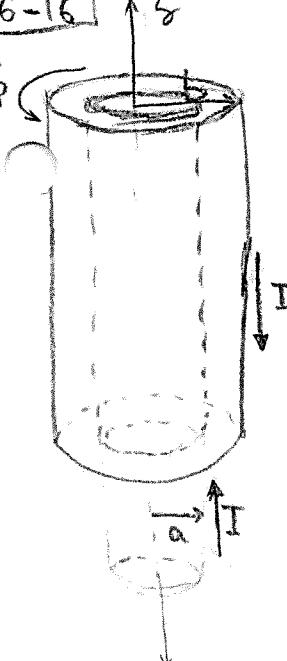
$$I_{\text{enc}} = 0 \Rightarrow \oint \vec{H} \cdot d\vec{l} = 0 \quad \text{overall paths} \Rightarrow \vec{H} = \vec{0}.$$

$$\text{inside } \vec{M} = ks \hat{z} \quad \text{and} \quad \vec{H} = \frac{1}{\mu_0} (\vec{B} - ks \hat{z}) = \vec{0} \Rightarrow \boxed{\vec{B}_{\text{in}} = \mu_0 ks \hat{z}}$$

$$\text{outside } \vec{M} = \vec{0} \quad \text{and as} \quad \vec{H} = \frac{1}{\mu_0} (\vec{B} - \vec{0}) = \frac{\vec{B}}{\mu_0} \Rightarrow \boxed{\vec{B}_{\text{out}} = \vec{0}} \quad \checkmark$$

good

6-16

Find \vec{B} between the tubes, a material of χ_m fills that space.

$$\oint \vec{H} \cdot d\vec{l} = N_{\text{turns}} \Rightarrow H(2\pi s) = I \Rightarrow \vec{H} = \frac{I}{2\pi s} \hat{\phi}$$

$$\vec{H} = \frac{1}{N_0} \vec{B} - \vec{M} = \frac{1}{N_0} \vec{B} - \chi_m \vec{H} \Rightarrow \vec{G} = (\vec{H} + \chi_m \vec{H}) N_0$$

$$\Rightarrow \vec{B} = N_0 (1 + \chi_m) \vec{H} = N_0 (1 + \chi_m) \frac{I}{2\pi s} \hat{\phi}$$

$$\Rightarrow \boxed{\vec{B} = N_0 (1 + \chi_m) \frac{I}{2\pi s} \hat{\phi} = \frac{NI}{2\pi s} \hat{\phi}}$$

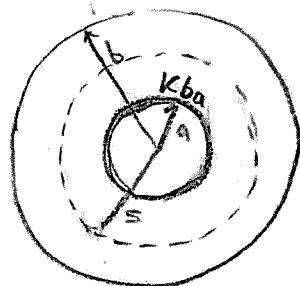
$$\vec{M} = \chi_m \vec{H} = \chi_m \frac{I}{2\pi s} \hat{\phi} = \vec{M}$$

"CHECK"

$$\vec{J}_s = \nabla \times \vec{M} = \nabla \times \chi_m \vec{H} = \frac{\chi_m I}{2\pi} \left(\nabla \times \frac{\hat{\phi}}{s} \right) = \frac{\chi_m I}{2\pi} \left(\frac{1}{s} \frac{\partial}{\partial s} \left(\frac{1}{s} \hat{\phi} \right) \right)_s = \vec{0}$$

$$\vec{K}_{BA} = \vec{M} \times \hat{n}_A = \chi_m \vec{H} \times (\hat{s}) = \frac{\chi_m I}{2\pi s} (\hat{\phi} \times (\hat{s})) = + \frac{\chi_m I}{2\pi s} \hat{z} \Big|_{s=a} = + \frac{\chi_m I}{2\pi a} \hat{z} = \vec{K}_{BA}$$

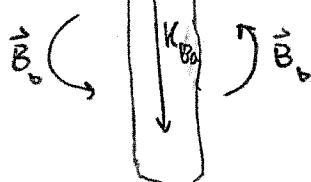
$$\oint \vec{B}_f \cdot d\vec{l} = N_0 I_f \Rightarrow \vec{B}_{\text{free}} = \frac{N_0 I}{2\pi s}$$



$$\oint \vec{B}_0 \cdot d\vec{l} = N_0 I_{\text{bound}} = N_0 (2\pi a) \frac{\chi_m I}{2\pi a} R(\chi)$$

$$\Rightarrow \vec{B}_0 (2\pi s) = N_0 (-\chi_m I)$$

$$\Rightarrow \vec{B}_0 = - \frac{N_0 \chi_m I}{2\pi s} \hat{\phi} \quad \checkmark$$



$$\vec{B}_{\text{free}} + \vec{B}_0 = \left\{ \frac{N_0 I}{2\pi s} + \frac{N_0 \chi_m I}{2\pi s} \right\} \hat{\phi}$$

$$= \frac{N_0 I}{2\pi s} \left\{ 1 + \chi_m \right\} \hat{\phi}$$

$$= N_0 (1 + \chi_m) \frac{I}{2\pi s} \hat{\phi} = \boxed{\frac{N_0 I}{2\pi s} \hat{\phi} = \vec{B}_{\text{total}}}$$