

9.1

(iv)

$$\begin{aligned}\frac{\partial^2 f_4}{\partial z^2} &= \frac{\partial^2}{\partial z^2} \left(A e^{-b(bz^2 + vt)} \right) = A \frac{\partial}{\partial z} \left(e^{-b(bz^2 + vt)} (-2bz) \right) \\ &= A e^{-b(bz^2 + vt)} \left[(-2bz)(-2bz) - 2b^2 z \right] \\ &= A e^{-b(bz^2 + vt)} \left[(2bz)^2 - 2b^2 z \right]\end{aligned}$$

$$\begin{aligned}\frac{1}{v^2} \frac{\partial^2 f_4}{\partial t^2} &= \frac{A}{v^2} \frac{\partial}{\partial t} \left(e^{-b(bz^2 + vt)} (-bv) \right) = \frac{A}{v^2} \left(e^{-b(bz^2 + vt)} (-bv)(-bv) \right) \\ &= A b^2 e^{-b(bz^2 + vt)} \neq A b^2 e^{-b(bz^2 + vt)} [4b^2 z^2 - 2] = \frac{\partial^2 f_4}{\partial z^2}\end{aligned}$$

✓ unless $1 = 4b^2 z^2 - 2 \Leftrightarrow z = \left(\frac{3}{4} \frac{1}{b^2}\right)^{1/2}$ certainly not $\forall t, z$ as we would like.

(v)

$$\begin{aligned}\frac{\partial^2 f_5}{\partial z^2} &= \frac{\partial^2}{\partial z^2} \left(A \sin(bz) \cos(bvt)^3 \right) = A \frac{\partial}{\partial z} \left(b \cos(bz) \cos(bvt)^3 - 0 \right) \\ &= A b \left(-(\sin bz) b \cos(bvt)^3 + \cos(bz) (0)^3 \right) = -A b^2 \sin(bz) \cos(bvt)^3\end{aligned}$$

$$\begin{aligned}\frac{1}{v^2} \frac{\partial^2 f_5}{\partial t^2} &= \frac{A}{v^2} \frac{\partial}{\partial t} \left(\left[\sin bz (-\sin(bvt)^3) 3(bvt)^2 bv \right] + \left[0 \cdot \cos(bvt)^3 \right] \right) \\ &= -\frac{A}{v^2} 3bv \sin bz \frac{\partial}{\partial t} \left((bvt)^2 \sin(bvt)^3 \right) \\ &= -\frac{A}{v^2} 3bv \sin bz \left(\partial(bvt) bv \sin(bvt)^3 + (bvt)^2 3(bvt) (bv) \cos(bvt)^3 \right) \\ &= -\frac{A}{v^2} 3bv \sin bz \left(2b^2 v^2 t \sin(bvt)^3 + 3bv (bvt)^4 \cos(bvt)^3 \right) \\ &= -3Ab^3 v \sin bz \sin(bvt)^3 + 9Ab^2 \frac{1}{v} \sin bz (bvt)^4 \cos(bvt)^3 \\ &= -3Ab^3 v \sin bz \sin(bvt)^3 + 9Av^3 b^6 t^4 \sin(bz) \cos(bvt)^3 \\ &\neq \frac{\partial^2 f_5}{\partial z^2} \text{ by the principle of gross disfigurement.}\end{aligned}$$

✓

9.2

(a) $f(z, t) = A \sin(kz) \cos(kvt)$

$$\frac{\partial^2 f}{\partial z^2} = \frac{\partial}{\partial z} (Ak \cos(kz) \cos(kvt)) = -\cos(kvt) Ak^2 \sin(kz)$$

$$\begin{aligned} \frac{1}{v^2} \frac{\partial^2 f}{\partial t^2} &= \frac{1}{v^2} A \sin(kz) (-kv) \frac{\partial}{\partial t} (\sin(kvt)) = \frac{-1}{v^2} Ak^2 v^2 \cos(kvt) \sin(kz) \\ &= -\cos(kvt) Ak^2 \sin(kz) \therefore \frac{\partial^2 f}{\partial z^2} = \frac{1}{v^2} \frac{\partial^2 f}{\partial t^2} \checkmark \end{aligned}$$

(b) find g, h such that $f(z, t) = g(z-vt) + h(z+vt)$

$$f = A \sin(kz) \cos(kvt)$$

↑
the variables g, h
depend on.

$$\sin(A+B) = \sin A \cos B + \sin B \cos A$$

$$\sin(A-B) = \sin A \cos B - \sin B \cos B$$

$$\frac{\sin(A+B) + \sin(A-B)}{2} = \sin A \cos B$$

Let $A = kz$
 $B = kvt$

then $\Rightarrow f = \frac{A}{2} (\sin(kz + kvt) + \sin(kz - kvt))$

$\checkmark$ thus $f = \frac{A}{2} \sin(kz + kvt) + \frac{A}{2} \sin(kz - kvt)$

Note/

$$h(z+vt) = \frac{A}{2} \sin(kz + kvt)$$

$$g(z-vt) = \frac{A}{2} \sin(kz - kvt)$$

9.3

20/20

$$A_3 e^{i\delta_3} = A_2 e^{i\delta_2} + A_1 e^{i\delta_1} \quad \text{Eq. 9.19}$$

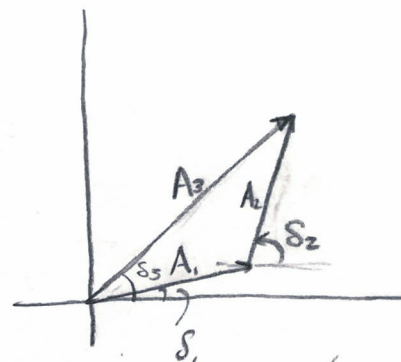
$$I \quad A_3 (\cos \delta_3 + i \sin \delta_3) = A_2 (\cos \delta_2 + i \sin \delta_2) + A_1 (\cos \delta_1 + i \sin \delta_1)$$

$$\text{Re}(I) = A_3 \cos \delta_3 = A_2 \cos \delta_2 + A_1 \cos \delta_1 \quad (*)$$

$$\text{Im}(I) = A_3 \sin \delta_3 = A_2 \sin \delta_2 + A_1 \sin \delta_1 \quad (**)$$

$$\frac{A_3 \sin \delta_3}{A_3 \cos \delta_3} = \tan \delta_3 = \frac{A_1 \sin \delta_1 + A_2 \sin \delta_2}{A_1 \cos \delta_1 + A_2 \cos \delta_2}$$

$$\checkmark \quad \therefore \delta_3 = \tan^{-1} \left\{ \frac{A_1 \sin \delta_1 + A_2 \sin \delta_2}{A_1 \cos \delta_1 + A_2 \cos \delta_2} \right\}$$



see just vector addition, break apart and add.

Complex conjugate of eq 9.19 $\Rightarrow$

$$A_3 e^{i\delta_3} = A_2 e^{i\delta_2} + A_1 e^{i\delta_1}$$

$$A_3 e^{-i\delta_3} = A_2 e^{-i\delta_2} + A_1 e^{-i\delta_1}$$

$$\begin{aligned} (A_3 e^{i\delta_3})(A_3 e^{-i\delta_3}) &= (A_2 e^{i\delta_2} + A_1 e^{i\delta_1})(A_2 e^{-i\delta_2} + A_1 e^{-i\delta_1}) \\ &= A_2^2 + A_1^2 + A_1 A_2 e^{i(\delta_1 - \delta_2)} + A_2 A_1 e^{-i(\delta_2 - \delta_1)} \\ &= A_2^2 + A_1^2 + A_1 A_2 (e^{i(\delta_1 - \delta_2)} + e^{-i(\delta_1 - \delta_2)}) \frac{1}{2} \cdot 2 \\ A_3^2 &= A_2^2 + A_1^2 + 2 A_1 A_2 \cos(\delta_1 - \delta_2) \end{aligned}$$

$$\checkmark \quad \therefore A_3 = (A_2^2 + A_1^2 + 2 A_1 A_2 \cos(\delta_1 - \delta_2))^{1/2} = (A_1^2 + A_2^2 + 2 A_1 A_2 \cos(\delta_2 - \delta_1))^{1/2}$$

by PLA!

(Principle of least astonishment)

or symmetry or $\cos X = \cos(-X)$.

note the above is easily obtained by the application of the law of cosines

9.4

SUPPOSE WE MAY COMPOSE OUR SOLUTION TO THE WAVE Eq. with
THE SUM OF A PRODUCT OF $z(z)$ and $y(t)$.

$$f(z, t) = z(z) y(t) \quad \text{Def}^n \quad z' = \frac{\partial z}{\partial z} \quad \text{and} \quad y' = \frac{\partial y}{\partial t}$$

$$\frac{\partial^2 f}{\partial z^2} = \frac{1}{v^2} \frac{\partial^2 f}{\partial t^2} \Rightarrow y z'' = \frac{1}{v^2} z y''$$

thus, $\frac{z''}{z} = \frac{1}{v^2} \frac{y''}{y} = \text{constant} = -\frac{\omega^2}{v^2}$, we know this must be constant
as $v \neq v(t)$ and y, z are independent.

$$z'' = -\frac{\omega^2}{v^2} z \Rightarrow z = c_1 e^{i(\frac{\omega}{v}z + \delta)}, \text{ where } c_1, \delta \text{ are arbitrary.}$$

$$y'' = -\omega^2 y \Rightarrow y = c_2 e^{i\omega t} + c_3 e^{-i\omega t}, \text{ where } c_2, c_3 \text{ are arbitrary}$$

Now since we are attempting to describe a finite
wave packet $\Rightarrow c_2 = 0$. Thus,

$$f(z, t) = z y = (c_1 e^{i(\frac{\omega}{v}z + \delta)}) c_3 e^{-i\omega t} \\ = c_1 c_3 e^{i\delta} e^{i(\frac{\omega}{v}z - \omega t)}$$

Note that $c_1 c_3 e^{i\delta} = \tilde{A}(k)$ since $\delta = \delta(k)$!
Then we compose some function " $\tilde{f}$ " as the
infinite sum of the multiplicative composition, Note $\frac{\omega}{v} \equiv k$.

$$\tilde{f} = \int_{-\infty}^{\infty} \tilde{A}(k) e^{i(kz - \omega t)} dk$$

cute

9.6

THIS STAPLE
THROUGH BOTH

BUT EACH ASSIGNMENT STAPLED SEPARATELY, PULL APART IF YOU WANT TO.

(a) $\Delta F = m \frac{\partial^2 f}{\partial t^2} \Big|_{z=0} = T \left(\frac{\partial f}{\partial z} \Big|_{0^+} - \frac{\partial f}{\partial z} \Big|_{0^-} \right)$ Boundary condition

38/40

derived from assumption θ small as in Book, we just know $\Delta F \neq 0$ rather $\Delta F = m f$

(b)
$$\tilde{f}(z, t) = \begin{cases} \tilde{A}_I e^{i(k_1 z - \omega t)} + \tilde{A}_R e^{(-k_1 z - \omega t)} & \text{for } z < 0 \\ \tilde{A}_T e^{i(k_2 z - \omega t)} & \text{for } z > 0 \end{cases}$$

$f(0^-, t) = f(0^+, t)$ for obvious reasons. Note $e^{ik_2 z} \rightarrow 1$ for $z \rightarrow 0$.

$\Rightarrow f(0^-, t) = \tilde{A}_I e^{-i\omega t} + \tilde{A}_R e^{-i\omega t} = \tilde{A}_T e^{-i\omega t} = \tilde{f}(0^+, t)$

$\therefore \tilde{A}_I + \tilde{A}_R = \tilde{A}_T$ (as before for $\Delta F = 0$)

$$\frac{\partial f}{\partial z} \Big|_{0^-} = ik_1 \tilde{A}_I e^{-i\omega t} - ik_1 \tilde{A}_R e^{-i\omega t}$$

$$\frac{\partial f}{\partial z} \Big|_{0^+} = ik_2 \tilde{A}_T e^{-i\omega t}$$

 (again e^z type terms $\rightarrow 0$ as $z \rightarrow 0$)

$$\frac{\partial^2}{\partial t^2} \left(\tilde{A}_T e^{i(k_2 z - \omega t)} \right) \Big|_{z=0} = -\tilde{A}_T \omega^2 e^{-i\omega t}$$

magnitude at $z=0$ must match $\tilde{A}_T = \tilde{A}_I + \tilde{A}_R$

$$\therefore -\frac{m\omega^2}{T} \tilde{A}_T = ik_2 \tilde{A}_T - ik_1 \tilde{A}_I + ik_1 \tilde{A}_R$$

$k_2 = \frac{\omega}{v_2}$ but $v_2 = \sqrt{\frac{T}{\mu_2}}$ however as $\mu_2 \rightarrow 0$ (massless) $\Rightarrow v_2 \rightarrow \infty \Rightarrow \underline{k_2 = 0}$

$$\therefore -\frac{m\omega^2}{T} \tilde{A}_T = -ik_1 \tilde{A}_I + ik_1 \tilde{A}_R$$

$10 \text{ cm} = 0.1 \text{ m} = \frac{1}{2} a t^2$
 $a = \frac{0.2}{(0.01)^2} = \frac{0.2}{0.0001} = 200 \text{ m/s}^2$

$v = at = 2000(0.01) = 20 \text{ m/s}$

$v = \sqrt{2gh}$
 $h = \frac{v^2}{2g}$

9.6

$$(b) \quad \tilde{A}_I + \tilde{A}_R = \tilde{A}_T$$

$$\frac{-m\omega^2}{T} \tilde{A}_T = -ik_1 \tilde{A}_I + ik_1 \tilde{A}_R$$

$$\Rightarrow \frac{-m\omega^2}{Tik} \tilde{A}_T = \tilde{A}_R - \tilde{A}_I = (\tilde{A}_T - \tilde{A}_I) - \tilde{A}_I$$

$$\therefore \tilde{A}_T \left(\frac{-m\omega^2}{Tik} - 1 \right) = -\tilde{A}_I$$

$$\tilde{A}_T \left(\frac{-m\omega^2 i}{\partial T k_1} + \frac{1}{2} \right) = \tilde{A}_I$$

$$\tilde{A}_T = \left(\frac{1}{2} - \frac{m\omega^2 i}{\partial T k_1} \right)^{-1} \tilde{A}_I$$

$$\frac{1}{2} - \frac{m\omega^2 i}{\partial T k_1} = \frac{-T k_1 - m\omega^2 i}{\partial T k_1} \left(\frac{T k_1 + m\omega^2 i}{T k_1 + m\omega^2 i} \right) = \frac{T^2 k_1^2 + m^2 \omega^4}{\partial T k_1 (T k_1 + m\omega^2 i)}$$

$$\tilde{A}_T = \left[\frac{\partial T^2 k_1^2}{T^2 k_1^2 + m^2 \omega^4} + i \frac{\partial T k_1 m \omega^2}{T^2 k_1^2 + m^2 \omega^4} \right] \tilde{A}_I$$

$$A_T e^{i\delta_T} = \frac{\partial T^2 k_1^2}{T^2 k_1^2 + m^2 \omega^4} A_I e^{i\delta_I}$$

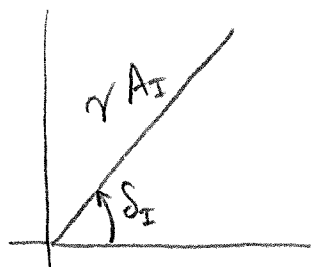
↑
γ

take Re part because

$N_2 < \mu$, and $V_2 > V_1$

$\Rightarrow$ phase $\delta_T = \delta_I$!

$\Rightarrow$ same phase ignore Im term.



$$A_T = \gamma A_I$$

$$\delta_T = \delta_I$$

by arguments of pg. 377!

5A_x

$$\tilde{A}_R = \tilde{A}_T - \tilde{A}_I = A_I(\gamma - 1)e^{i\delta_I}$$

$$\boxed{A_R = A_I(\gamma - 1)} \\ \boxed{\delta_R = \delta_I}$$

9.7

$$(a) T \frac{\partial^2 f}{\partial z^2} \Delta z - \gamma \Delta z \frac{\partial f}{\partial t} = \mu \Delta z \frac{\partial^2 f}{\partial t^2}$$

$$\Rightarrow \frac{\partial^2 f}{\partial z^2} - \frac{\gamma}{T} \frac{\partial f}{\partial t} - \frac{\mu}{T} \frac{\partial^2 f}{\partial t^2} = 0$$

$$(b) \delta \tilde{f}(z, t) = e^{i\omega t} \tilde{F}(z)$$

$$e^{i\omega t} \frac{\partial^2}{\partial z^2} (\tilde{F}(z)) - \frac{\gamma}{T} i\omega e^{i\omega t} \tilde{F}(z) + \frac{\mu}{T} \omega^2 e^{i\omega t} \tilde{F}(z) = 0$$

$$\frac{\partial^2}{\partial z^2} (\tilde{F}(z)) - i \frac{\gamma\omega}{T} \tilde{F}(z) + \frac{\mu\omega^2}{T} \tilde{F}(z) = 0$$

$$\frac{\partial^2}{\partial z^2} (\tilde{F}) = \left[i \frac{\gamma\omega}{T} + \frac{\mu\omega^2}{T} \right] \tilde{F} = -\beta^2 \tilde{F}(z)$$

$$\Rightarrow \tilde{F}(z) = a e^{i\beta z} + c e^{-i\beta z} = \tilde{\alpha} e^{i\beta z} = \tilde{F}(z)$$

$$\text{thus } \tilde{f}(z, t) = e^{i\omega t} \tilde{\alpha} e^{i\beta z} = \tilde{\alpha} e^{i(\omega t + \beta z)} = \tilde{f}(z, t)$$

$$-\beta^2 = i \frac{\gamma\omega}{T} + \frac{\mu\omega^2}{T} \Rightarrow \beta = \pm \left[-i \frac{\gamma\omega}{T} + \frac{\mu\omega^2}{T} \right]^{1/2}$$

$$(c) \tilde{f}(z, t) = \frac{1}{e} \tilde{f}(0, t), \text{ what is this } z?$$

$$e^{i\omega t} \tilde{\alpha} e^{0-1} = e^{i\omega t} \tilde{\alpha} e^{i\beta z}$$

$$\Rightarrow e^{-1} = e^{i\beta z} \Rightarrow i\beta z = -1 \Rightarrow \beta z = \frac{-1}{i}$$

$$z = \frac{i}{\left(\frac{\mu\omega^2}{T} - i \frac{\gamma\omega}{T} \right)^{1/2}} = \frac{\text{Re} \left(i \left(\frac{\mu\omega^2}{T} - i \frac{\gamma\omega}{T} \right)^{1/2} \right)}{\left(\frac{\mu^2\omega^4}{T^2} + \frac{\gamma^2\omega^2}{T^2} \right)^{1/2}}$$

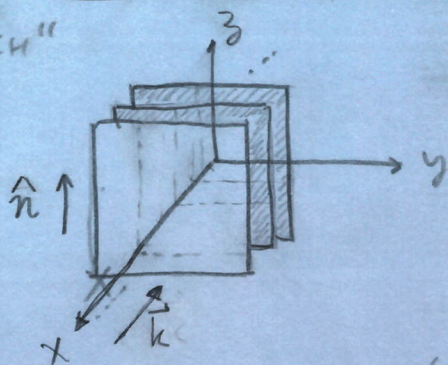
9.9

(a) Describe Plane wave's E, B if it has $\delta=0$ and polarization in $\hat{z}$ and travels in x . By analogy to book,

$$E(x,t) = E_0 \cos(-kx - \omega t) \hat{z}$$

$$B(x,t) = \frac{E_0}{c} \cos(-kx - \omega t) \hat{y}$$

"sketch"



these planes represent
max's in waves
 2π apart.

Directions Check easily by,

$$\vec{B}_0 = \frac{\vec{k} \times \vec{E}_0}{\omega}$$

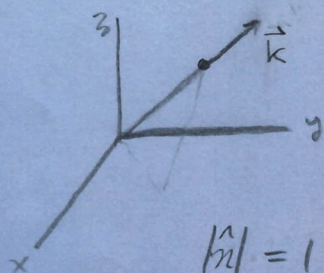
$$\omega \vec{B}_0 = \vec{k} \times \vec{E}_0$$

$$\omega \frac{E_0}{c} \hat{y} = \vec{k} \times E_0 \hat{z}$$

$$\vec{k} = -\frac{\omega}{c} \hat{x}$$

$$\hat{n} = \hat{z}$$

(b) $\vec{r} = x\hat{i} + y\hat{j} + z\hat{k}$



$$\vec{k} = \frac{k}{\sqrt{3}}(\hat{i} + \hat{j} + \hat{k})$$

$$\hat{k} \cdot \hat{n} = \frac{1}{\sqrt{3}}(\hat{i} + \hat{j} + \hat{k}) \cdot (\alpha\hat{i} + \gamma\hat{k})$$

$$= \frac{1}{\sqrt{3}}(\alpha + \gamma) = 0 \Rightarrow \alpha = -\gamma$$

all // vectors
to x-y plane
 $\neq \Delta y$!

$$|\hat{n}| = 1 \Rightarrow$$

$$\hat{n} = \frac{1}{\sqrt{2}}(\hat{i}) - \frac{1}{\sqrt{2}}(\hat{k})$$

$$\left\{ \begin{array}{l} k_x = k_y = k_z \\ k = \frac{\omega}{c} \end{array} \right\} \Rightarrow$$

$$\vec{k} = \frac{\omega}{\sqrt{3}c}(\hat{i} + \hat{j} + \hat{k})$$

9.9

(b) Direction of $\vec{B}$?

$$\hat{k} \times \hat{n} = \frac{1}{\sqrt{3}}(i+j+k) \times \frac{1}{\sqrt{2}}(i-k)$$

$$= \frac{1}{\sqrt{6}}(j-k-i+j) = \frac{1}{\sqrt{6}}(2j-k-i) = \hat{k} \times \hat{n}$$

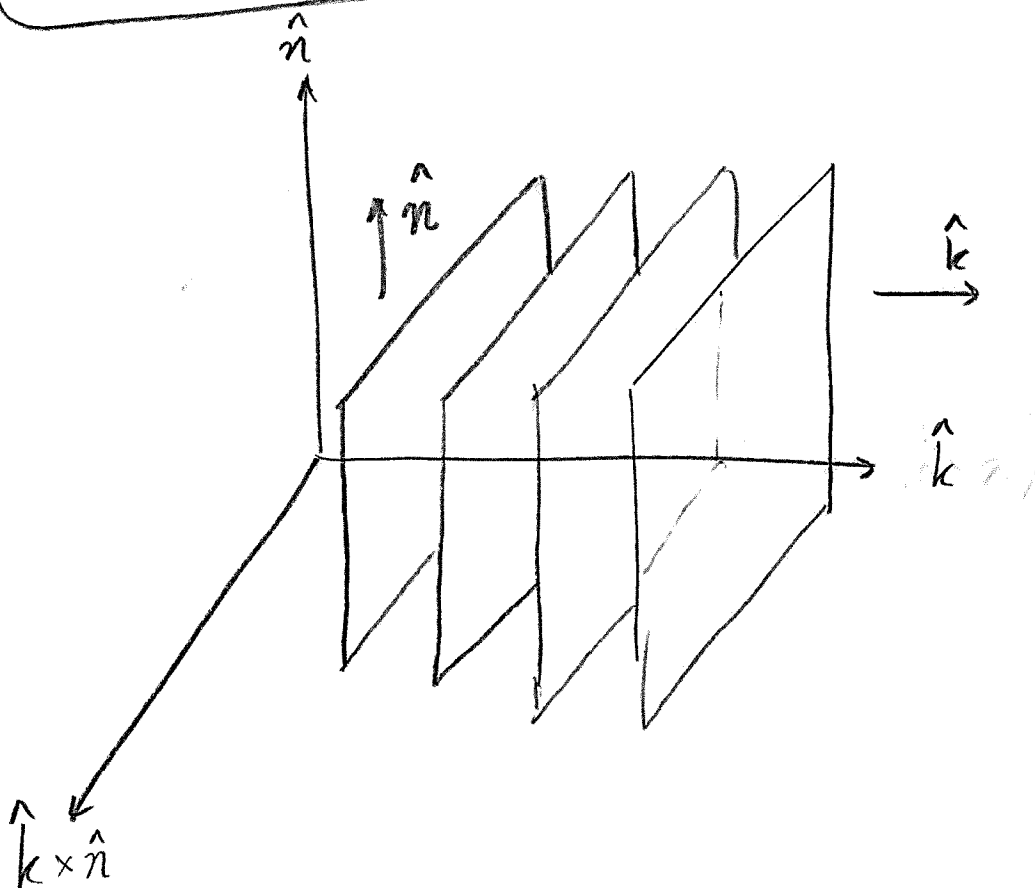
$$\vec{k} \cdot \vec{r} = \frac{\omega}{\sqrt{3}c}(i+j+k) \cdot (xi+yj+zk)$$

$$= \frac{\omega}{\sqrt{3}c}(x+y+z)$$

∴ BY ANALOGY TO BOOK

$$\vec{E}(x, y, z, t) = E_0 \cos\left(\frac{\omega}{c\sqrt{3}}(x+y+z) - \omega t\right) \hat{n}$$

$$\vec{B}(x, y, z, t) = \frac{E_0}{c} \cos\left(\frac{\omega}{c\sqrt{3}}(x+y+z) - \omega t\right) (\hat{k} \times \hat{n})$$



9.10

$$I = 1300 \text{ W/m}^2$$



PERFECT
ABSORBER

ON A PERFECT ABSORBER

$$P_A = \frac{I}{c} = \frac{1300 \text{ W/m}^2}{3 \times 10^8 \text{ m/s}} = \boxed{4.33 \times 10^{-6} \text{ PA} = P_{\text{Abs.}}}$$

ON A PERFECT REFLECT

$$P_R = \frac{2I}{c} = \frac{2 \times 1300 \text{ W/m}^2}{3 \times 10^8 \text{ m/s}} = \boxed{8.67 \times 10^{-6} \text{ PA} = P_{\text{REFLECT}}}$$

ATMOSPHERIC PRESSURE = 101,325 PA.

$$\checkmark \frac{P_R}{P_{\text{ATMOS}}} = \frac{8.67 \times 10^{-6}}{1.01325 \times 10^5} = \boxed{8.55 \times 10^{-11} = \frac{P_R}{P_{\text{ATMOS}}}}$$

$\Rightarrow 8.55 \times 10^{-9} \% \text{ of } P_{\text{ATMOS.}}$

9-16 Analyze polarization $\perp$ to plane of incidence (ie E in $\hat{y}$ for fig. 9.15)

IMPOSE 9.101.

20/20

(i) not much here no E^+ , no E in $\hat{z}$

(ii) $(\tilde{B}_{oI} + \tilde{B}_{oR})_z = (\tilde{B}_{oT})_z$ where $\tilde{B}_o = \frac{1}{v} \hat{k} \times \tilde{E}_o \Rightarrow \tilde{B}_o = \frac{k}{v}$

$$\tilde{B}_{oI} = \frac{1}{v_1} \hat{k}_I \times \tilde{E}_{oI} = \frac{1}{v_1} k_I \tilde{E}_{oI} (\cos \theta_I (\hat{z} \times \hat{y}) + \sin \theta_I (\hat{x} \times \hat{y})) = \frac{k_I}{v_1} \tilde{E}_{oI} (-\cos \theta_I \hat{x} + \sin \theta_I \hat{z})$$

$$\tilde{B}_{oR} = \frac{1}{v_1} \hat{k}_R \times \tilde{E}_{oR} = \frac{1}{v_1} k_R \tilde{E}_{oR} (\cos \theta_R (\hat{z} \times \hat{y}) + \sin \theta_R (\hat{x} \times \hat{y})) = \frac{k_R}{v_1} \tilde{E}_{oR} (\cos \theta_R \hat{x} + \sin \theta_R \hat{z})$$

$$\tilde{B}_{oT} = \frac{1}{v_2} \hat{k}_T \times \tilde{E}_{oT} = \frac{k_T}{v_2} \tilde{E}_{oT} (\cos \theta_T (\hat{z} \times \hat{y}) + \sin \theta_T (\hat{x} \times \hat{y})) = \frac{k_T}{v_2} \tilde{E}_{oT} (-\cos \theta_T \hat{x} + \sin \theta_T \hat{z})$$

now that I have found the B 's lets apply iii. note $\vec{k} \neq \hat{k}$!

$$\frac{1}{v_1} \tilde{E}_{oI} \sin \theta_I - \frac{1}{v_1} \tilde{E}_{oR} \sin \theta_R = \frac{1}{v_2} \tilde{E}_{oT} \sin \theta_T$$

(iii) $(\tilde{E}_{oI} + \tilde{E}_{oR})_{x,y} = (\tilde{E}_{oT})_{x,y}$

by assumption $\tilde{E}_{oI}$ in y direction, from last hunk $\Rightarrow \tilde{E}_{oR}$ also in $y \therefore \tilde{E}_{oT}$ in y !
that is $\tilde{E}_{oI} + \tilde{E}_{oR} = \tilde{E}_{oT}$ where all directions but y are zero for E .

(iv) $\frac{1}{\mu_1} (\tilde{B}_{oI} + \tilde{B}_{oR})_{x,y} = \frac{1}{\mu_2} (\tilde{B}_{oT})_{x,y}$, as E is in $y \Rightarrow B$ must be in x these are linear media $\therefore E \perp B$!
(also in z but who cares here)

$$\frac{1}{\mu_1} \left(-\frac{\tilde{E}_{oI}}{v_1} \cos \theta_I + \frac{\tilde{E}_{oR}}{v_1} \cos \theta_R \right) = \frac{1}{\mu_2} \left(-\frac{\tilde{E}_{oT}}{v_2} \cos \theta_T \right)$$

$$\frac{\cos \theta_I}{\mu_1 v_1} (\tilde{E}_{oI} - \tilde{E}_{oR}) = \frac{\cos \theta_T}{\mu_2 v_2} (\tilde{E}_{oT})$$

9-16

$$\beta \equiv \frac{\mu_1 v_1}{\mu_2 v_2} = \frac{\mu_1 n_2}{\mu_2 n_1} \quad \text{and} \quad \alpha \equiv \frac{\cos \theta_T}{\cos \theta_I}$$

from (iii) $\tilde{E}_{oI} + \tilde{E}_{oR} = \tilde{E}_{oT}$

from (iv) $\frac{\cos \theta_I}{\mu_1 v_1} (\tilde{E}_{oI} - \tilde{E}_{oR}) = \frac{\cos \theta_T}{\mu_2 v_2} (\tilde{E}_{oT})$

$$\Rightarrow \frac{\cos \theta_T}{\cos \theta_I} (\tilde{E}_{oT}) = \frac{\mu_2 v_2}{\mu_1 v_1} (\tilde{E}_{oI} - \tilde{E}_{oR})$$

$$\Rightarrow \alpha \tilde{E}_{oT} = \frac{1}{\beta} (\tilde{E}_{oI} - \tilde{E}_{oR})$$

$$\therefore \alpha \beta (\tilde{E}_{oI} + \tilde{E}_{oR}) = (\tilde{E}_{oI} - \tilde{E}_{oR})$$

$$\Rightarrow \boxed{\tilde{E}_{oR} = \frac{(1 - \alpha \beta)}{(1 + \alpha \beta)} \tilde{E}_{oI}} =$$

OR $\alpha \tilde{E}_{oT} = \frac{1}{\beta} (\tilde{E}_{oI} - (\tilde{E}_{oT} - \tilde{E}_{oI}))$
 $= \frac{1}{\beta} (2\tilde{E}_{oI} - \tilde{E}_{oT})$

$$(\alpha \beta + 1) \tilde{E}_{oT} = 2\tilde{E}_{oI}$$

$$\Rightarrow \boxed{\tilde{E}_{oT} = \left(\frac{2}{\alpha \beta + 1} \right) \tilde{E}_{oI}}$$

Brewster's 4 / I tried 2 ways.

if $\tilde{E}_{oR} = 0 \Rightarrow (1 - \alpha \beta) \tilde{E}_{oI} = 0 \Rightarrow \text{as } \tilde{E}_{oI} \neq 0, 1 = \alpha \beta, \alpha = \frac{1}{\beta}$

$\therefore \tilde{E}_{oT} = \left(\frac{2}{1+1} \right) \tilde{E}_{oI} \Rightarrow \tilde{E}_{oT} = \tilde{E}_{oI}$ (optically indistinguishable!)

$$\alpha = \frac{\cos \theta_T}{\cos \theta_I} = \frac{\sqrt{1 - \left(\frac{n_1}{n_2}\right)^2 \sin^2 \theta_I}}{\cos \theta_I} = \frac{1}{\beta} = \frac{\mu_2 n_1}{\mu_1 n_2} = \frac{n_1}{n_2} \quad (\text{if } \mu_1 = \mu_2)$$

$$\Rightarrow 1 - \left(\frac{n_1}{n_2}\right)^2 \sin^2 \theta_I = \left(\frac{n_1}{n_2}\right)^2 \cos^2 \theta_I = \cos^2 \theta_I + \sin^2 \theta_I - \sin^2 \theta_I \left(\frac{n_1}{n_2}\right)^2 = \left(\frac{n_1}{n_2}\right)^2 \cos^2 \theta_I$$

$$\Rightarrow \left(\frac{n_1}{n_2}\right)^2 \Rightarrow n_1^2 = n_2^2$$

again the only case for no reflection is just the trivial case of not changing media.

9-16

Confirming Proper forms for Fresnel Eq's.

$$\tilde{E}_{or} = \left(\frac{1 - \alpha\beta}{1 + \alpha\beta} \right) \tilde{E}_{oi}$$

$$\tilde{E}_{ot} = \left(\frac{2}{\alpha\beta + 1} \right) \tilde{E}_{oi}$$

at normal incidence $\theta_i = \theta_r = \theta_t = 0$! $\therefore \alpha = \frac{\cos \theta_t}{\cos \theta_i} = \frac{1}{1} = 1$.

thus $\boxed{\tilde{E}_{or} = \left(\frac{1 - \beta}{1 + \beta} \right) \tilde{E}_{oi}}$

and $\boxed{\tilde{E}_{ot} = \left(\frac{2}{1 + \beta} \right) \tilde{E}_{oi}}$

R and T

$$R = \frac{I_r}{I_i} = \frac{\frac{1}{2} \epsilon_1 v_1 \tilde{E}_{or}^2}{\frac{1}{2} \epsilon_1 v_1 \tilde{E}_{oi}^2} = \left(\frac{1 - \alpha\beta}{1 + \alpha\beta} \right)^2 = R$$

$$T = \frac{I_t}{I_i} = \frac{\frac{1}{2} \epsilon_2 v_2 \cos \theta_t \tilde{E}_{ot}^2}{\frac{1}{2} \epsilon_1 v_1 \cos \theta_i \tilde{E}_{oi}^2} \frac{\epsilon_2 v_2}{\epsilon_1 v_1} \left(\frac{2}{1 + \alpha\beta} \right)^2$$

$$= \alpha \frac{v_2 \left(\frac{1}{\mu_2 v_2^2} \right)}{v_1 \left(\frac{1}{\mu_1 v_1^2} \right)} \left(\frac{2}{1 + \alpha\beta} \right)^2 = \frac{\mu_1 v_1}{\mu_2 v_2} \left(\frac{2}{1 + \alpha\beta} \right)^2$$

$$= \boxed{\alpha\beta \left(\frac{2}{1 + \alpha\beta} \right)^2 = T}$$

$$\beta = \frac{\mu_1 v_1}{\mu_2 v_2} = \frac{\mu_1 n_2}{\mu_2 n_1}$$

$$v_i^2 = \frac{1}{\mu_i \epsilon_i} \Rightarrow \epsilon_i = \frac{1}{\mu_i v_i^2}$$

$$R + T = \left(\frac{1 - \alpha\beta}{1 + \alpha\beta} \right)^2 + \alpha\beta \left(\frac{2}{1 + \alpha\beta} \right)^2$$

$$= \frac{1 - 2\alpha\beta + (\alpha\beta)^2 + 4\alpha\beta}{(1 + \alpha\beta)^2}$$

$$= \frac{1 + 2\alpha\beta + (\alpha\beta)^2}{(1 + \alpha\beta)^2} = \frac{(1 + \alpha\beta)^2}{(1 + \alpha\beta)^2} = 1 \quad \therefore \boxed{R + T = 1}$$

9-16

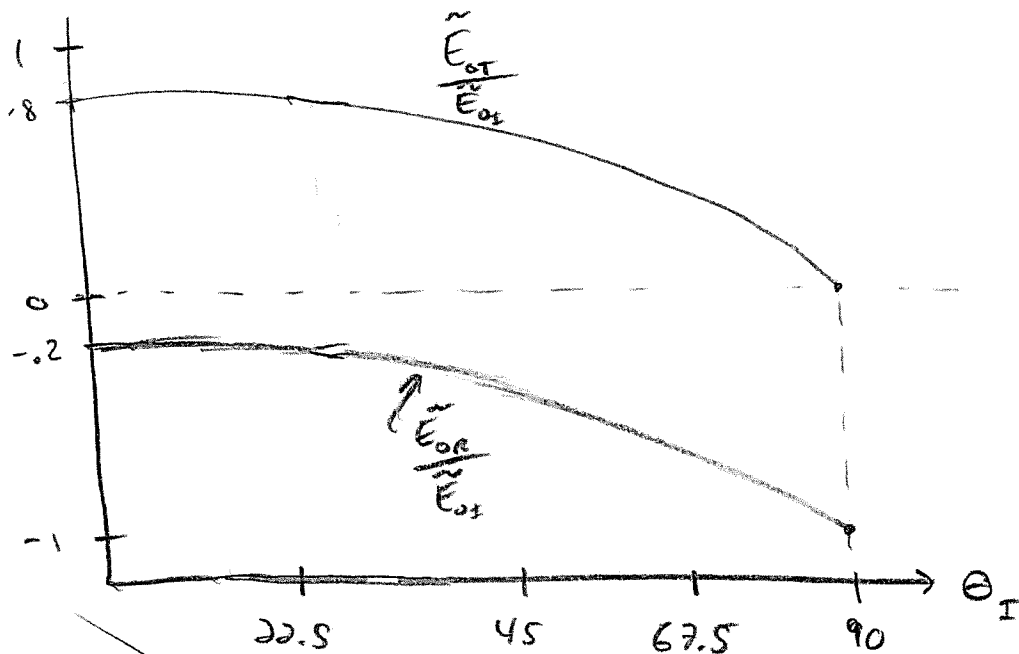
The "Sketch"

$$\alpha = \frac{\cos \theta_r}{\cos \theta_i} = \frac{\sqrt{1 - \left(\frac{1}{1.5}\right)^2 \sin^2 \theta_i}}{\cos \theta_i}$$

$$\frac{E_{or}}{E_{oi}} = \frac{1 - 1.5 \left(\frac{\sqrt{1 - \frac{\sin^2 \theta_i}{2.25}}}{\cos \theta_i} \right)}{1 + 1.5 \left(\frac{\sqrt{1 - \frac{\sin^2 \theta_i}{2.25}}}{\cos \theta_i} \right)}$$

$$\frac{E_{ot}}{E_{oi}} = \frac{2}{1 + 1.5 \left(\frac{\sqrt{1 + \frac{\sin^2 \theta_i}{2.25}}}{\cos \theta_i} \right)}$$

note $(1.5)^2 = 2.25$



9-17

$n_{\text{diamond}} = 2.42$. Construct analogous graph to 9.16 for $\epsilon_{0T}/\epsilon_{0I}$ vs. $\epsilon_{0R}/\epsilon_{0I}$!
 air / diamond interface. First calculate, (assume $\mu_0 = \mu_1 = \mu_2$)

(a) Amplitudes at normal incidence $\alpha = \frac{\cos \theta_T}{\cos \theta_I} = 1$, $\beta = \frac{\mu_1 n_2}{n_1 n_1} = \frac{n_2}{n_1} = 2.42$

$$\tilde{E}_{0R} = \left(\frac{\alpha - \beta}{\alpha + \beta} \right) \tilde{E}_{0I} = \frac{1 - \beta}{1 + \beta} \tilde{E}_{0I} = \frac{1 - 2.42}{3.42} \tilde{E}_{0I} = \frac{-1.58}{3.42} \tilde{E}_{0I} = \boxed{-.415 \tilde{E}_{0I} = \tilde{E}_{0R}}$$

$$\tilde{E}_{0T} = \left(\frac{2}{\alpha + \beta} \right) \tilde{E}_{0I} = \frac{2}{3.42} \tilde{E}_{0I} = \boxed{0.585 \tilde{E}_{0I} = \tilde{E}_{0T}}$$

(b) $\tilde{E}_{0R} = 0$ for Brewster's angle.

$$0 = \left(\frac{\alpha - \beta}{\alpha + \beta} \right) \tilde{E}_{0I} \Rightarrow (\alpha - \beta) \tilde{E}_{0I} = 0 \Rightarrow \alpha - \beta = 0 \Rightarrow \underline{\alpha = \beta}$$

and as the book nicely derives we know if $\mu_1 \neq \mu_2 \Rightarrow n_1 \neq n_2$
 thus $\beta \neq n_1/n_2 \Rightarrow \sin^2 \theta_B \neq \beta^2 / (1 + \beta^2) \therefore$

$$\tan \theta_B = \frac{n_2}{n_1} \Rightarrow \theta_B = \tan^{-1}(2.42) = \boxed{67.5^\circ = \theta_B}$$

(c) crossover angle, $\tilde{E}_{0R} = \tilde{E}_{0T}$

$$\Rightarrow \tilde{E}_{0T} = \left(\frac{2}{\alpha + \beta} \right) \tilde{E}_{0I} = \left(\frac{\alpha - \beta}{\alpha + \beta} \right) \tilde{E}_{0I} = \tilde{E}_{0R}$$

$$\Rightarrow \frac{2}{\alpha + \beta} = \frac{\alpha - \beta}{\alpha + \beta} \Rightarrow 2 = \alpha - \beta = \alpha - 2.42$$

$$\therefore \alpha = 4.42 = \frac{\cos \theta_T}{\cos \theta_I} = \frac{\sqrt{1 - \left(\frac{n_1}{n_2} \right)^2 \sin^2 \theta_I}}{\cos \theta_I} = \sqrt{1 - \frac{1}{\beta^2} \sin^2 \theta_I}$$

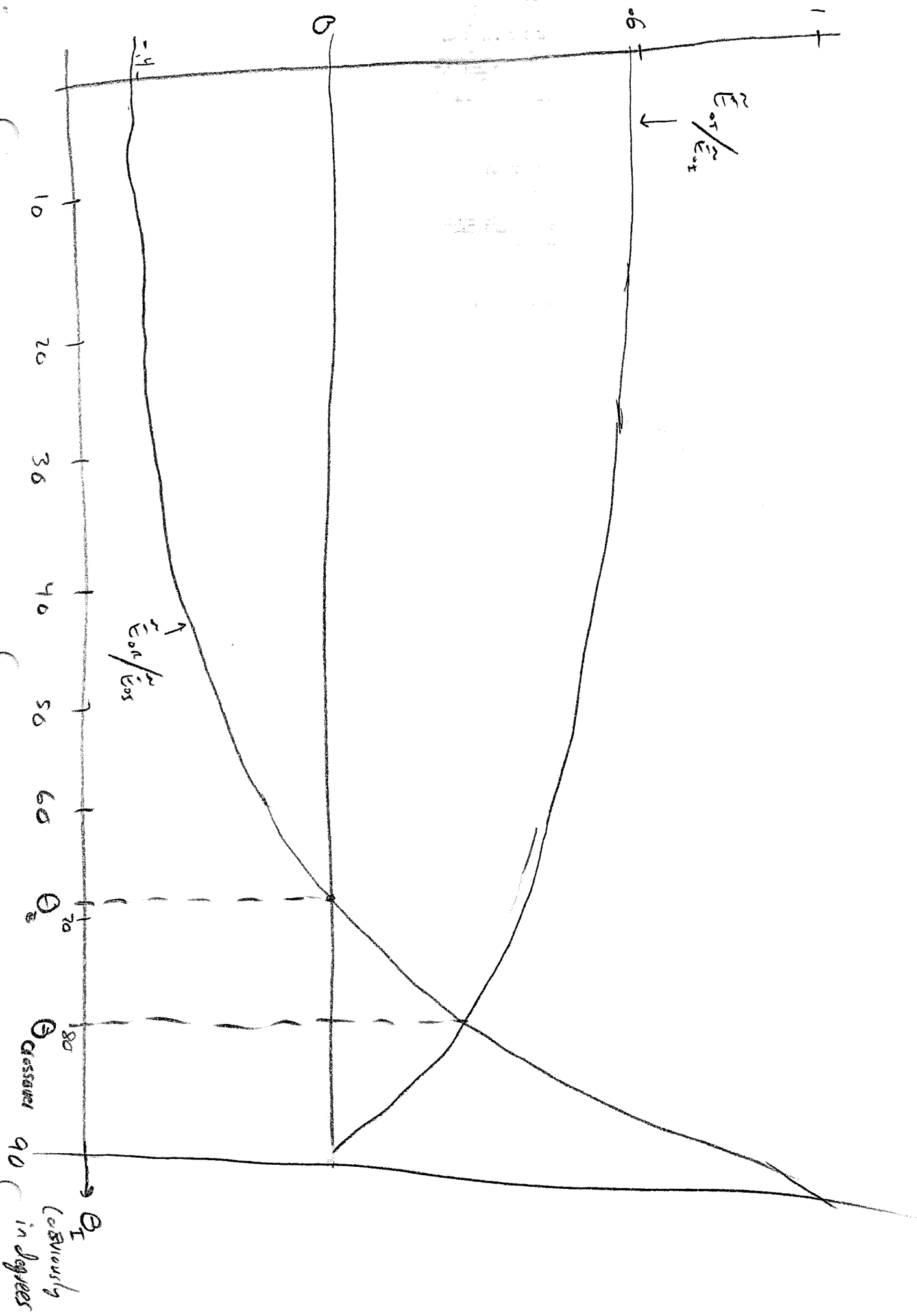
$$\begin{aligned} (2 + \beta)^2 \cos^2 \theta_I &= 1 - \frac{1}{\beta^2} \sin^2 \theta_I \\ &= 1 - \frac{1}{\beta^2} (1 - \cos^2 \theta_I) \end{aligned}$$

$$.171 = \frac{1}{\beta^2}$$

$$\cos^2 \theta_I \left((2 + \beta)^2 - \frac{1}{\beta^2} \right) = 1 - \frac{1}{\beta^2}$$

$$\cos \theta_I = \left(\frac{1 - 1/\beta^2}{(2 + \beta)^2 - 1/\beta^2} \right)^{1/2}$$

$$\theta_I = \cos^{-1} \left[\left(\frac{1 - 1/\beta^2}{(2 + \beta)^2 - 1/\beta^2} \right)^{1/2} \right] = \cos^{-1}(.2069) = \boxed{78.06^\circ = \theta_I}$$



9-19

(a) Show that skin depth in poor conductor ($\sigma \ll \omega\epsilon$) is $\frac{2}{\sigma} \sqrt{\frac{\epsilon}{\mu}}$ independent of frequency. Find skin depth for water.

$$d = \frac{1}{k}, \quad k = \omega \sqrt{\frac{\epsilon\mu}{2} \left[\sqrt{1 + \left(\frac{\sigma}{\epsilon\omega}\right)^2} - 1 \right]^{1/2}}$$

$$(1+x)^n = 1 + nx + \dots \Rightarrow k = \omega \sqrt{\frac{\epsilon\mu}{2} \left[1 + \frac{1}{2} \left(\frac{\sigma}{\epsilon\omega}\right)^2 - 1 \right]^{1/2}}$$

$$\therefore k = \omega \sqrt{\frac{\epsilon\mu}{2}} \left(\sqrt{\frac{1}{2}} \frac{\sigma}{\epsilon\omega} \right) = \sqrt{\frac{\mu\sigma^2}{4\epsilon}} = \frac{\sigma}{2} \sqrt{\frac{\mu}{\epsilon}}$$

$$d = \frac{1}{k} = \frac{2}{\sigma} \sqrt{\frac{\epsilon}{\mu}}$$

$$d = \frac{2}{\sigma} \sqrt{\frac{\epsilon}{\mu}} \approx 20 \sqrt{\frac{\epsilon_0}{\mu_0}} = (2(0.5 \times 10^5) \sqrt{\frac{8.854 \times 10^{-12}}{4\pi \times 10^{-7}}}) \text{ m} = d = 11,869 \text{ m}$$

(b) Show $d = \frac{2}{\sigma\pi}$ when $\sigma \gg \omega\epsilon$

$$k = \omega \sqrt{\frac{\epsilon\mu}{2} \left[\sqrt{1 + \left(\frac{\sigma}{\epsilon\omega}\right)^2} - 1 \right]^{1/2}} \xrightarrow{\sigma \gg \omega\epsilon} k = \omega \sqrt{\frac{\epsilon\mu}{2}} \sqrt{\frac{\sigma}{\epsilon\omega}}$$

$$k = \omega \sqrt{\frac{\mu\sigma}{2\omega}} = \sqrt{\frac{\omega\mu\sigma}{2}} \Rightarrow d = \sqrt{\frac{2}{\omega\mu\sigma}}$$

$$k = \omega \sqrt{\frac{\epsilon\mu}{2} \left[\sqrt{1 + \left(\frac{\sigma}{\epsilon\omega}\right)^2} + 1 \right]^{1/2}} \xrightarrow{\sigma \gg \omega\epsilon} k = \omega \sqrt{\frac{\epsilon\mu}{2}} \sqrt{\frac{\sigma}{\epsilon\omega}} = \sqrt{\frac{\omega\mu\sigma}{2}}$$

$$d = \sqrt{\frac{2}{\omega\mu\sigma}} = \frac{1}{k} = \frac{1}{\frac{\sigma}{2\pi}} = \frac{2}{\sigma\pi} = d$$

if $\sigma \approx 10^7 (\Omega\text{m})^{-1}$, $\omega \approx 10^{15} \text{ s}^{-1}$ and $\epsilon = \epsilon_0$, $\mu = \mu_0$.

$$\Rightarrow d = \left(\frac{2}{10^{15} \cdot 4\pi \cdot 10^{-7} \cdot 10^7} \right)^{1/2} \text{ m} = 12.6 \times 10^{-9} \text{ m} \approx d$$

the metal is opaque because light can not penetrate the metal very appreciably. The distance it would take for the light to drop to $\approx 98\%$ of its surface strength would be a mere $5d \approx 60 \text{ nm}$

9.21 Calculate the reflection coefficient for light at an air-to-silver interface ($\mu_1 = \mu_2 = \mu_0$, $\epsilon_1 = \epsilon_0$, $\sigma = 6 \times 10^7 (\Omega m)^{-1}$ with $\omega = 4 \times 10^{15} / s$.

$$R \equiv \frac{I_R}{I_i} = \left(\frac{E_{0R}}{E_{0i}} \right)^2 = \left(\frac{1 - \tilde{\beta}}{1 + \tilde{\beta}} \right)^2$$

$$\tilde{\beta} = \frac{\mu_1 v_1}{\mu_2 \omega} \tilde{k}_2 = \frac{v_1}{\omega} \tilde{k}_2 \approx \frac{c}{\omega} \tilde{k}_2$$

$$\tilde{k} = k + iK \Rightarrow \tilde{\beta} = \alpha k + i\alpha K$$

$$\begin{aligned} R &= \left(\frac{1 - \tilde{\beta}}{1 + \tilde{\beta}} \right)^* \left(\frac{1 - \tilde{\beta}}{1 + \tilde{\beta}} \right) = \frac{\left(\frac{1 - \alpha k + i\alpha K}{1 + \alpha k - i\alpha K} \right) \left(\frac{1 - \alpha k - i\alpha K}{1 + \alpha k + i\alpha K} \right)}{\left(\frac{1 - \alpha k - i\alpha K}{1 + \alpha k + i\alpha K} \right) \left(\frac{1 - \alpha k + i\alpha K}{1 + \alpha k - i\alpha K} \right)} \\ &= \frac{(1 - \alpha k - i\alpha K)(1 - \alpha k + i\alpha K)}{(1 + \alpha k + i\alpha K)(1 + \alpha k - i\alpha K)} \\ &= \frac{1 - \alpha k - \alpha k + \alpha^2 k^2 + \alpha^2 K^2}{1 + \alpha k + \alpha k + \alpha^2 k^2 + \alpha^2 K^2} \\ &= \frac{1 - 2\alpha k + \alpha^2 k^2 + \alpha^2 K^2}{1 + 2\alpha k + \alpha^2 k^2 + \alpha^2 K^2} \end{aligned}$$

$$k = \omega \sqrt{\frac{\epsilon \mu}{2}} \left[\sqrt{1 + \left(\frac{\sigma}{\omega \epsilon} \right)^2} + 1 \right]^{1/2}$$

$$K = \omega \sqrt{\frac{\epsilon \mu}{2}} \left[\sqrt{1 + \left(\frac{\sigma}{\omega \epsilon} \right)^2} - 1 \right]^{1/2}$$

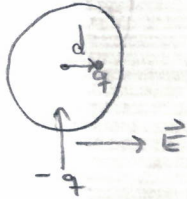
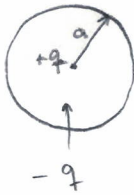
note $\omega \sqrt{\frac{\epsilon \mu}{2}} = \frac{\omega}{c\sqrt{2}}$

$$R = \frac{1 - 2\frac{\omega}{c\sqrt{2}} \left[\sqrt{1 + \left(\frac{\sigma}{\omega \epsilon} \right)^2} + 1 \right]^{1/2} + \frac{\omega^2}{c^2} \frac{1}{2} \left[\sqrt{1 + \left(\frac{\sigma}{\omega \epsilon} \right)^2} + 1 \right] + \frac{\omega^2}{c^2} \frac{1}{2} \left[\sqrt{1 + \left(\frac{\sigma}{\omega \epsilon} \right)^2} - 1 \right]}{1 + 2\frac{\omega}{c\sqrt{2}} \left[\sqrt{1 + \left(\frac{\sigma}{\omega \epsilon} \right)^2} + 1 \right]^{1/2} + \frac{\omega^2}{c^2} \frac{1}{2} \left[\sqrt{1 + \left(\frac{\sigma}{\omega \epsilon} \right)^2} + 1 \right] + \frac{\omega^2}{c^2} \frac{1}{2} \left[\sqrt{1 + \left(\frac{\sigma}{\omega \epsilon} \right)^2} - 1 \right]}$$

$$R = \frac{1 - \sqrt{2} \left[\sqrt{1 + \left(\frac{\sigma}{\omega \epsilon} \right)^2} + 1 \right]^{1/2} + \gamma}{1 + \sqrt{2} \left[\sqrt{1 + \left(\frac{\sigma}{\omega \epsilon} \right)^2} + 1 \right]^{1/2} + \gamma} = \frac{1 - \sqrt{2} \left(\sqrt{1 + \left(\frac{\sigma}{\omega \epsilon} \right)^2} + 1 \right)^{1/2} + \sqrt{1 + \left(\frac{\sigma}{\omega \epsilon} \right)^2}}{1 + \sqrt{2} \left(\sqrt{1 + \left(\frac{\sigma}{\omega \epsilon} \right)^2} + 1 \right)^{1/2} + \sqrt{1 + \left(\frac{\sigma}{\omega \epsilon} \right)^2}} = \boxed{-0.9989 = R}$$

9.23

TAKE MODEL EX. 4.1, what natural frequency do you get?



15/20

$$E_e = \frac{1}{4\pi\epsilon_0} \frac{qd}{a^3} = E \Rightarrow p = qd = (4\pi\epsilon_0 a^3) E$$

$$\therefore \alpha = 4\pi\epsilon_0 a^3 = 3\epsilon_0(\text{Volume})$$

$$F_{\text{binding}} = -k_{\text{spring}} x = -m\omega_0^2 x$$

ω_0 = natural oscillation frequency

$$F_{\text{damping}} = -m\gamma \frac{dx}{dt}$$

$$F_{\text{driving}} = qE = qE_0 \cos(\omega t)$$

$$m \frac{d^2 x}{dt^2} = F_{\text{total}} = F_{\text{bind}} + F_{\text{damp.}} + F_{\text{driving}}$$

electron as damped harm. osc. with massive nucleus assumed at rest
NO DAMPING HERE,

$$F_{\text{bind}} = F_{\text{driv}} \Rightarrow m\omega_0^2 d = qE_e = \frac{q^2 d}{4\pi\epsilon_0 a^3}$$

$$\omega_0^2 = \frac{q^2}{m 4\pi\epsilon_0 a^3} \Rightarrow \omega_0 = \sqrt{\frac{q^2}{4\pi\epsilon_0 m a^3}}$$

$$\omega_0 = \sqrt{\frac{q^2}{4\pi\epsilon_0 m a^3}}$$

$$\omega_0 = \left(\frac{(1.6 \times 10^{-19})^2}{(4 \times \pi \times 8.852 \times 10^{-12}) (9.11 \times 10^{-31}) (0.5 \times 10^{-10})^3} \right)^{1/2} \text{ s}^{-1} = 4.5 \times 10^{16} \frac{\text{rad}}{\text{s}} = \omega_0$$

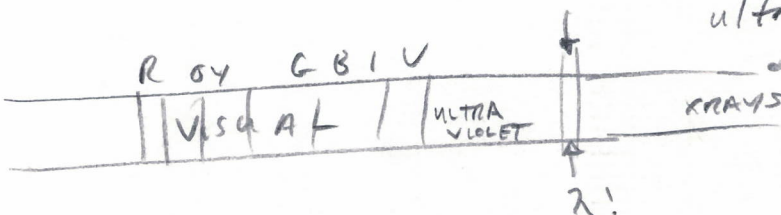
$$f_0 = \frac{\omega_0}{2\pi} = 7.15 \times 10^{15} \text{ Hz} = f_0$$

$$\lambda = \frac{c}{f_0}$$

$$\lambda = 41.9 \text{ nm}$$

$\Rightarrow$ in very low x-ray or very high energy ultraviolet region depending

which way you like to look at it.



9.23

Find Coefficients of ref. and disp., comp. to Hyd.

JAMES COOK

$$A = 1.36 \times 10^{-4}, \quad B = 7.7 \times 10^{-15} \text{ m}^2$$

$$n = 1 + \left(\frac{Nq^2}{2m\epsilon_0} \sum_j \frac{f_j}{\omega_j^2} \right) + \omega^2 \left(\frac{Nq^2}{2m\epsilon_0} \sum_j \frac{f_j}{\omega_j^4} \right) \quad \omega^2 = \frac{4\pi^2 c^2}{\lambda^2}$$

$$n = 1 + \frac{Nq^2}{2m\epsilon_0} \left(\frac{1}{\omega_0^2} + \frac{4\pi^2 c^2}{\omega_0^2 \lambda^2} \right) = 1 + A \left(1 + \frac{B}{\lambda^2} \right)$$

$$\rightarrow \cancel{A} = \frac{Nq^2}{2m\epsilon_0 \omega_0^2} = \frac{3q^2}{8m\epsilon_0 \omega_0^2 r^3 \pi} = \boxed{1.50 = A}$$

$$B = \frac{4\pi^2 c^2}{\omega_0^2} = \boxed{1.75 \times 10^{-15} = B} \quad \downarrow$$

$$A_{\text{got}} \approx 10,000 A_{\text{HYD.}}$$

$$B_{\text{got}} \approx 4.5 B_{\text{HYD.}}$$

9.24

Find the width of the anomalous dispersion region for case of single resonance freq. ω_0 , assume $\gamma \ll \omega_0$

Show that the index of refraction assumes min/max values at points where absorption coeff is at $\frac{1}{2}$ max.

$$\alpha \equiv 2K = \text{abs. coeff.}$$

$$\alpha = 2K \approx \frac{Nq^2\omega^2}{m\epsilon_0 c} \sum_j \frac{f_j \gamma_j}{(\omega_j^2 - \omega^2)^2 + \gamma_j^2 \omega^2} = \frac{Nq^2\omega^2}{m\epsilon_0 c} \frac{\gamma_0}{(\omega_0^2 - \omega^2)^2 + \gamma_0^2 \omega^2}$$

$$n \approx 1 + \frac{Nq^2}{2m\epsilon_0} \frac{(\omega_0^2 - \omega^2)}{(\omega_0^2 - \omega^2)^2 + \gamma_0^2 \omega^2} \equiv 1 + \delta \frac{\beta}{\beta^2 + \gamma^2} \quad \begin{aligned} \beta &= \omega_0^2 - \omega^2 \\ \gamma &= \gamma_0 \omega \end{aligned}$$

$$\begin{aligned} \frac{dn}{d\omega_0} &= \frac{dn}{d\beta} \frac{d\beta}{d\omega_0} = \delta \frac{d\beta}{d\omega_0} \frac{d}{d\beta} \left(\frac{\beta}{\beta^2 + \gamma^2} \right) & \frac{d\beta}{d\omega_0} &= 2\omega_0 \\ &= \delta 2\omega_0 \left(\frac{1}{\beta^2 + \gamma^2} - \frac{\beta}{(\beta^2 + \gamma^2)^2} \frac{d}{d\beta} (\beta^2 + \gamma^2) \right) & \frac{d}{d\omega_0} \beta^2 + \frac{d}{d\omega_0} \gamma^2 &= 0 \\ & & \frac{d}{d\omega_0} \beta^2 &= 2\beta 2\omega_0 \end{aligned}$$

$$\textcircled{0} \text{ (max, min)} = \delta 2\omega_0 \left(\frac{1}{\beta^2 + \gamma^2} - \frac{\beta}{(\beta^2 + \gamma^2)^2} 2\beta \right)$$

$$\frac{1}{\beta^2 + \gamma^2} = \frac{2\beta^2}{(\beta^2 + \gamma^2)^2} \Rightarrow 1 - \frac{2\beta^2}{\beta^2 + \gamma^2} = 0$$

$$\beta^2 + \gamma^2 - 2\beta^2 = 0 \Rightarrow \beta^2 = \gamma^2$$

$$(\omega_0^2 - \omega^2)^2 = (\gamma \omega)^2 \Rightarrow \omega_0 = \pm \sqrt{\omega^2 + \gamma \omega}$$

$$\omega_2 = \sqrt{\omega^2 + \gamma \omega} \quad \omega_1 = -\sqrt{\omega^2 + \gamma \omega}$$

$$\omega_2 - \omega_1 = 2\sqrt{\omega^2 + \gamma \omega} = \text{width between max and min where the anomalous disp happens}$$

-4

9.25 Show $v_g < c$ even when $v > c$.

Given $\gamma_j = 0 \Rightarrow n = 1 + \frac{Nq^2}{2m\epsilon_0} \sum_j \frac{f_j}{\omega_j^2 - \omega^2} = \frac{ck}{\omega}$

10/10

$$\therefore k = \left[\omega + \frac{Nq^2}{2m\epsilon_0} \sum_j \frac{f_j \omega}{\omega_j^2 - \omega^2} \right] \frac{1}{c} \quad \text{Let } \delta = \frac{Nq^2}{2m\epsilon_0}$$

$$\begin{aligned} \frac{1}{v_g} = \frac{dk}{d\omega} &= \frac{1}{c} \frac{d}{d\omega} \left\{ \omega + \delta \sum_j \frac{f_j \omega}{\omega_j^2 - \omega^2} \right\} \quad \text{Let } \delta_j = \frac{\delta}{c} \sum_j \\ &= \frac{1}{c} + \delta_j \frac{d}{d\omega} \left(\omega (\omega_j^2 - \omega^2)^{-1} \right) \\ &= \frac{1}{c} + \delta_j \left\{ (\omega_j^2 - \omega^2)^{-1} - \omega (\omega_j^2 - \omega^2)^{-2} (2\omega) \right\} \quad \text{Let } \beta = (\omega_j^2 - \omega^2) \\ &= \frac{1}{c} + \delta_j \left\{ \beta^{-1} + 2\omega^2 \beta^{-2} \right\} \\ &= \frac{1}{c} + \delta_j \left\{ \frac{\beta + 2\omega^2}{\beta^2} \right\} \quad \text{note } \beta + 2\omega^2 = \omega_j^2 + \omega^2 \end{aligned}$$

$$\therefore v_g = \frac{1}{\frac{1}{c} + \delta_j \left\{ \frac{\beta + 2\omega^2}{\beta^2} \right\}} = \frac{1}{\frac{1}{c} + \underbrace{\frac{Nq^2}{2m\epsilon_0 c} \sum_j \left[\frac{\omega_j^2 + \omega^2}{(\omega_j^2 - \omega^2)^2} \right]}_Q}$$

$$v_g = \frac{1}{\frac{1}{c} + Q} \Rightarrow v_g(1 + QC) = c$$

$$\therefore v_g > c \iff 1 + QC < 1 \Rightarrow v_g > c \text{ only if } QC < 0.$$

Thus all that remains is for me to show that $QC \geq 0$

Then v_g cannot be greater than c !

$$QC = \frac{Nq^2 c}{2m\epsilon_0 c} \sum_j \left[\frac{\omega_j^2 + \omega^2}{(\omega_j^2 - \omega^2)^2} \right], \text{ then note, } N, q^2, m, \epsilon_0, \omega_j^2, \omega^2, (\omega_j^2 - \omega^2)^2 > 0$$

And as we know the sum of positive numbers is positive, thus $QC > 0$

$\therefore v_g$ is necessarily less than c , Even if $v > c$.

hence nothing to