

1.) If $V, W \in \mathbb{X}(\mathbb{R}^3)$ which are point-wise LI then show that $E_1 = \frac{1}{\|V\|} V$, $E_2 = \frac{1}{\|\tilde{W}\|} \tilde{W}$, $E_3 = E_1 \times E_2$ is a frame field where $\tilde{W} = W - \text{Proj}_V(W) = \text{Orth}_V(W)$.

Observe $E_i \cdot E_j = 1$ by construction. Moreover $E_1 \cdot E_2 = 1$ by construction, consider, $V, W \neq 0$ as $\{V, W\}$ is LI at each p ,

$$\begin{aligned} E_1 \cdot E_2 &= \frac{1}{\|V\|} \frac{1}{\|\tilde{W}\|} V \cdot \left[W - \frac{(W \cdot V)}{\|V \cdot V\|} V \right] = \\ &= \frac{1}{\|V\|} \frac{1}{\|\tilde{W}\|} \left(V \cdot W - \frac{(W \cdot V)(V \cdot V)}{\|V \cdot V\|} \right) \\ &= 0. \end{aligned}$$

Finally $\|E_3\| = \|E_1\| \|E_2\| \sin 90^\circ = 1$ and $E_1 \cdot E_3 = E_2 \cdot E_3 = 0$ by construction of $E_3 = E_1 \times E_2$. Hence $\{E_1, E_2, E_3\}$ forms a frame field on \mathbb{R}^3 .

Remark: this was point-wise Gram-Schmidt paired with cross-product technique.

2.) Express the vector fields below in terms of

(i.) cylindrical frame with r, θ, z -based coefficients

(ii.) spherical frame with ρ, θ, ϕ -based coeff. formulas.

$$(a.) U_1 = (U_1 \cdot E_1) E_1 + (U_1 \cdot E_2) E_2 + (U_1 \cdot \overset{0}{E_3}) E_3 = \cos \theta E_1 - \sin \theta E_2$$

$$U_1 = (F_1 \cdot U_1) F_1 + (F_2 \cdot U_1) F_2 + (F_3 \cdot U_1) F_3 = \cos \alpha \cos \theta F_1 + \underbrace{\sin \alpha \cos \theta F_2}_{\theta - \sin \alpha \cos \theta F_3} +$$

Recall the following to do the calculations above,

$$E_1 = \cos \theta U_1 + \sin \theta U_2$$

$$E_2 = -\sin \theta U_1 + \cos \theta U_2$$

$$E_3 = U_3$$

$$F_1 = \cos \phi (\cos \theta U_1 + \sin \theta U_2) + \sin \phi U_3$$

$$F_2 = -\sin \phi (\cos \theta U_1 + \sin \theta U_2)$$

$$F_3 = -\sin \theta (\cos \phi U_1 + \sin \phi U_2) + \cos \phi U_3$$

$$2b) \cos\theta U_1 + \sin\theta U_2 + U_3 = \Sigma$$

$$\Sigma = (\Sigma \cdot E_1) E_1 + (\Sigma \cdot E_2) E_2 + (\Sigma \cdot E_3) E_3$$

$$\Rightarrow \Sigma = (\cos^2\theta + \sin^2\theta) E_1 + (-\sin\theta \cos\theta + \cos\theta \sin\theta) E_2 + E_3 \\ = \underline{E_1 + E_3}.$$

$$\Sigma = (\Sigma \cdot F_1) F_1 + (\Sigma \cdot F_2) F_2 + (\Sigma \cdot F_3) F_3$$

$$= (\cos^2\theta \cos\phi + \sin^2\theta \cos\phi + \sin\phi) F_1 + (-\sin\theta \cos\theta + \sin\theta \cos\theta) F_2 + \\ \quad \swarrow + (-\sin\phi \cos^2\theta - \sin\phi \sin^2\theta + \cos\phi) F_3$$

$$= \underline{\underline{(\cos\phi + \sin\phi) F_1 + (\cos\phi - \sin\phi) F_3}}.$$

$$2c.) \Sigma = x U_1 + y U_2 + z U_3$$

$$\Sigma = (\Sigma \cdot E_1) E_1 + (\Sigma \cdot E_2) E_2 + (\Sigma \cdot E_3) E_3$$

$$= (x \cos\theta + y \sin\theta) E_1 + (-x \sin\theta + y \cos\theta) E_2 + z E_3$$

$$= (r \cos^2\theta + r \sin^2\theta) E_1 + (-r \cos\theta \sin\theta + r \sin\theta \cos\theta) E_2 + z E_3$$

$$= \underline{r E_1 + z E_3}. \quad (\text{neat simplification})$$

$$\Sigma = (\Sigma \cdot F_1) F_1 + (\Sigma \cdot F_2) F_2 + (\Sigma \cdot F_3) F_3$$

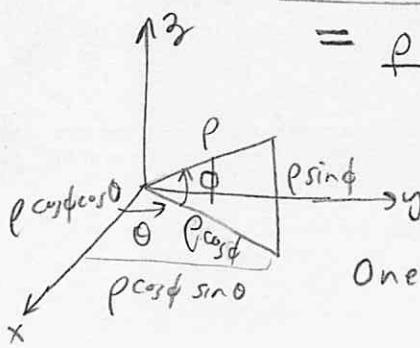
$$= (x \cos\phi \cos\theta + y \cos\phi \sin\theta + z \sin\phi) F_1 +$$

$$\swarrow + (-x \sin\theta + y \cos\theta) F_2 + (-x \sin\phi \cos\theta - y \sin\phi \sin\theta + z \cos\phi) F_3$$

$$= (\rho \cos^2\phi \cos^2\theta + \rho \sin^2\phi \cos^2\theta + \rho \sin^2\phi) F_1 + (-\rho \cos\phi \cos\theta \sin\theta + \rho \sin\phi \cos\theta \sin\theta) F_2 +$$

$$\swarrow + (-\rho \cos\phi \cos^2\theta \sin\theta - \rho \sin\phi \cos\phi \sin^2\theta + \rho \sin\phi \cos\phi) F_3$$

$$= \underline{\rho F_1}.$$



O'Neill's Nonstandard Sphericals

(3.) Find frame field E_1, E_2, E_3 such that

$$E_1 = \cos(x) U_1 + \sin(x) \cos(z) U_2 + \sin(x) \sin(z) U_3$$

Notice $E_1 \cdot E_1 = \cos^2 x + \sin^2 x \cos^2 z + \sin^2 x \sin^2 z = 1$, good.

The answer here would not seem to be unique. That said, the following should suffice,

$$E_2 = \sin(x) U_1 - \cos(x) \cos(z) U_2 - \cos(x) \sin(z) U_3$$

Clearly $E_2 \cdot E_2 = 1$. Also, $E_1 \cdot E_2 = \sin(x) \cos(x) [1 - \cos^2 z - \sin^2 z] = 0$.

Then, we obtain E_3 via $E_3 = E_1 \times E_2$,

$$E_1 \times E_2 = \begin{vmatrix} U_1 & U_2 & U_3 \\ \omega x & \sin x \cos z & \sin x \sin z \\ \sin x & -\cos x \cos z & -\cos x \sin z \end{vmatrix}$$

$$= (0) U_1 - (-\cos^2 x \sin z - \sin^2 x \sin z) U_2 + (-\cos^2 x \cos z - \sin^2 x \cos z) U_3$$

$$= [\sin z U_2 - \cos z U_3] = E_3$$

§2.7 #1 Let $E_1 = \frac{1}{\sqrt{2}} (\sin f U_1 + U_2 - \cos f U_3)$

$$E_2 = \frac{1}{\sqrt{2}} (\sin f U_1 - U_2 - \cos f U_3)$$

$$E_3 = \cos f U_1 + \sin f U_3$$

} show these form a frame field and find its connection forms

You can easily verify $E_i \cdot E_j = \delta_{ij}$ $\forall i, j \in \{1, 2, 3\}$. Observe the attitude matrix A and dA yield $\omega = (dA) A^T$,

$$A = \frac{1}{\sqrt{2}} \begin{bmatrix} \sin f & 1 & -\cos f \\ \sin f & -1 & -\cos f \\ \sqrt{2} \cos f & 0 & \sqrt{2} \sin f \end{bmatrix} \hookrightarrow dA = \frac{1}{\sqrt{2}} \begin{bmatrix} \cos f df & 0 & \sin f df \\ \cos f df & 0 & \sin f df \\ -\sqrt{2} \sin f df & 0 & \sqrt{2} \cos f df \end{bmatrix}$$

$$\omega = (dA) A^T = dA \frac{1}{\sqrt{2}} \begin{bmatrix} \sin f & \sin f & \sqrt{2} \cos f \\ 1 & -1 & 0 \\ -\cos f & -\cos f & \sqrt{2} \sin f \end{bmatrix} = \begin{bmatrix} 0 & \omega_{12} & \omega_{13} \\ -\omega_{12} & 0 & \omega_{23} \\ -\omega_{13} & -\omega_{23} & 0 \end{bmatrix}$$

$$\Rightarrow \omega_{12} = \cancel{\sin f \cos f df} - \cancel{\cos f \sin f df} = 0, \quad \omega_{13} = (\cos^2 f df + \sin^2 f df) / \sqrt{2} = \frac{df}{\sqrt{2}}$$

$$\omega_{23} = \frac{-\sin^2 f df - \cos^2 f df}{\sqrt{2}} = -\frac{df}{\sqrt{2}} \quad \therefore \left(\omega = \frac{1}{\sqrt{2}} \begin{bmatrix} 0 & 0 & df \\ 0 & 0 & -df \\ -df & df & 0 \end{bmatrix} \right)$$

[§2.7#2] Find the connection forms of U_1, U_2, U_3

(HSI)

Observe $A = I \Rightarrow dA = 0 \Rightarrow \omega = dAA^T = 0$.

[§2.7#3] For any function f , show A below is the attitude matrix of a frame field, calculate the connection forms

$$A = \begin{bmatrix} \cos^2 f & \cos f \sin f & \sin f \\ \sin f \cos f & \sin^2 f & -\cos f \\ -\sin f & \cos f & 0 \end{bmatrix} \quad A^T = \begin{bmatrix} \cos^2 f & \sin f \cos f & -\sin f \\ \cos f \sin f & \sin^2 f & \cos f \\ \sin f & -\cos f & 0 \end{bmatrix}$$

You can multiply to verify $AA^T = I$ (we need this to confirm orthonormality for the frame which A forms attitude)

$$dA = \begin{bmatrix} -2\cos f \sin f df & (\cos^2 f - \sin^2 f) df & \cos f df \\ (\cos^2 f - \sin^2 f) df & 2\sin f \cos f df & \sin f df \\ -\cos f df & -\sin f df & 0 \end{bmatrix}$$

To calculate connection forms find $(1,2), (1,3), (2,3)$ components for $\omega = dA A^T$,

$$\omega_{12} = (\cos^2 f, \cos f \sin f, \sin f) \cdot ((\cos^2 f - \sin^2 f) df, 2\sin f \cos f df, \sin f df)$$

$$\omega_{12} = (\cos^4 f - \sin^2 f \cos^2 f + 2\sin^2 f \cos^2 f + \sin^4 f) df$$

$$= (\underline{\cos^2 f \cos^2 f} + \underline{\cos^4 f \sin^2 f} + \underline{\sin^2 f}) df \Rightarrow \boxed{\omega_{12} = df}$$

$$\omega_{13} = (-\cos^2 f \cos f - \sin^2 f \cos f) df \Rightarrow \boxed{\omega_{13} = -\cos f df}$$

$$\omega_{23} = (-\sin f (\cos^2 f - \sin^2 f) + 2\cos^2 f \sin f) df$$

$$= (\sin^3 f + \sin f \cos^2 f) df$$

$$= \sin f df \therefore \boxed{\omega_{23} = \sin f df}$$

this disagrees
with text, I
wonder if

you all
will agree
with me or
Oneil...
I've likely
made a
mistake in
here...

$$\boxed{\omega = \begin{bmatrix} 0 & 1 & -\cos f \\ -1 & 0 & \sin f \\ \cos f & -\sin f & 0 \end{bmatrix} df}$$

§2.7 #4, I leave to you

(typo in text)

(H52)

§2.7 #5 Let $W = \sum_i f_i E_i$ and prove $\nabla_V W = \sum_j \left[V[f_j] + \sum_i f_i w_{ij}(V) \right] E_j$

$$\nabla_V W = \nabla_V \left(\sum_{i=1}^3 f_i E_i \right)$$

$$= \sum_{i=1}^3 \nabla_V (f_i E_i)$$

$$= \sum_{i=1}^3 \left(V[f_i] E_i + f_i \nabla_V E_i \right)$$

$$= \sum_{i=1}^3 \left(V[f_i] E_i + f_i \sum_{j=1}^3 w_{ij}(V) E_j \right)$$

$$= \sum_{i=1}^3 V[f_i] E_i + \sum_{i=1}^3 \sum_{j=1}^3 f_i w_{ij}(V) E_j$$

$$= \sum_{i=1}^3 V[f_i] E_i + \sum_{j=1}^3 \sum_{i=1}^3 f_j w_{ji}(V) E_i$$

$$= \sum_{i=1}^3 \left(V[f_i] + \sum_{j=1}^3 f_j w_{ji}(V) \right) E_i$$

$$= \sum_{j=1}^3 \left(V[f_j] + \sum_{i=1}^3 f_i w_{ij}(V) \right) E_j$$

∃ typo in O'neil here.

cylindrical connection

$$W = \begin{bmatrix} 0 & d\theta & 0 \\ -d\theta & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

§2.7 #6 Let E_1, E_2, E_3 be the cylindrical frame field, $V \in \mathcal{X}(\mathbb{R}^3)$ ↑ such that $V[r] = r$, $V[\theta] = 1$. Calculate $\nabla_V (r \cos \theta E_1 + r \sin \theta E_3)$

Use the result of (5.), $\hookrightarrow d\theta(V) = 1$

$$\begin{aligned} \nabla_V W &= V[r \cos \theta] E_1 + V[r \sin \theta] E_3 + f_1 w_{12}(V) E_2 + f_1 w_{13}(V) E_3 + 2 \\ &\quad + f_3 w_{31}(V) E_1 + f_3 w_{32}(V) E_2 \quad \text{or see pg. 92} \\ &= (\cos \theta V[r] - r \sin \theta V[\theta]) E_1 + (\sin \theta V[r] + r \cos \theta V[\theta]) E_3 + f_1 d\theta[V] E_2 \\ &= (r \cos \theta - r \sin \theta) E_1 + (r \sin \theta + r \cos \theta) E_3 + r \cos \theta E_2 \\ &= r(\cos \theta - \sin \theta) E_1 + r(\sin \theta + \cos \theta) E_3 + r \cos \theta E_2 \end{aligned}$$

§2.7 #8 Let β be unit-speed with $\kappa > 0$.

H53

β, E_1, E_2, E_3 is frame field on \mathbb{R}^3 s.t. when

E_1, E_2, E_3 restricted to β gives T, N, B of β . Prove

$$\omega_{12}(T) = \kappa, \quad \omega_{13}(T) = 0, \quad \omega_{23}(T) = \tau$$

We found in #5 of §2.5 the restriction of $W \in \mathcal{X}(\mathbb{R}^3)$ to $\alpha: I \subseteq \mathbb{R} \rightarrow \mathbb{R}^3$ given by $(W|_\alpha)(t) = W(\alpha(t)) = W_\alpha(t)$ had $\nabla_{\alpha'(t)} W = (W_\alpha)'(t)$. Note $\beta' = T$ for unit-speed and $\omega_{ij}(v) = (\nabla_v E_i) \circ E_j$ hence, at $\beta(t)$,

$$\begin{aligned} \omega_{12}(T) &= (\nabla_T E_1) \circ E_2(\beta(t)) \\ &= (\nabla_{\beta'(t)} E_1) \circ N \\ &= (E_1(\beta(t)))'(t) \circ N \\ &= T' \circ N \\ &= \kappa N \circ N \\ &= \boxed{\kappa}. \end{aligned} \quad \left. \begin{array}{l} E_1|_\beta = T \\ E_2|_\beta = N \\ E_3|_\beta = B \end{array} \right\}$$

$$\begin{aligned} \omega_{13}(T) &= (\nabla_T E_1) \circ E_3(\beta(t)) \\ &= T' \circ B \\ &= \kappa N \circ B \\ &= \boxed{0}. \end{aligned} \quad \left. \begin{array}{l} \text{details similar} \\ \text{to} \end{array} \right\}$$

$$\begin{aligned} \omega_{23}(T) &= (\nabla_T E_2) \circ E_3(\beta(t)) \\ &= (E_2(\beta(t)))' \circ B \\ &= N' \circ B \\ &= (-\kappa T + \tau B) \circ B \\ &= \boxed{\tau}. \end{aligned}$$

Remark: I'm curious, how would we calculate $\omega_{ij}(B)$ or $\omega_{ij}(N)$. We only see T -components here.

§2.7 #8 continued:

(HS4)

deduce Frenet formulas from connection eq^{hys}.

$$\nabla_V E_1 = \omega_{12}(V) E_2 + \omega_{13}(V) E_3$$

$$\nabla_V E_2 = -\omega_{12}(V) E_1 + \omega_{23}(V) E_3$$

$$\nabla_V E_3 = -\omega_{13}(V) E_1 - \omega_{23}(V) E_2$$

We know $E_1 = \beta' = T$, $E_2 = \frac{1}{\kappa} \beta'' = N$ and $E_3 = T \times N$ along β . The Frenet eq^{hys} $T' = \kappa N$ is essentially a def² so, I'm not sure what is meant by this problem... I'll try to play along, how can we find T' , N' , B' in connection eq^{hys}?

$$\nabla_{\alpha'(t)} W = W'_\alpha(t) \quad \text{exercise #5 of §2.5}$$

$$\hookrightarrow \nabla_T W = W' \text{ along } \beta \text{ for } W = E_1, E_2, E_3.$$

$$\nabla_T T = \omega_{12}(T) N + \omega_{13}(T) B = T' \rightarrow \underline{T' = \kappa N}.$$

$$\nabla_T N = -\omega_{12}(T) T + \omega_{23}(T) B = N' \rightarrow \underline{N' = -\kappa T + \tau B}.$$

$$\nabla_T B = -\omega_{13}(T) T - \omega_{23}(T) N = B' \rightarrow \underline{B' = -\tau N}.$$

I think this is what was intended here, note to find ω_{12} , ω_{13} , ω_{23} I need to know how T , N , B change in T , N , B directions... here's what I take away, the connection eq^{hys} are consistent with Frenet Serret as they restrict to appropriate frame on a $\kappa > 0$ curve.

1.) Let θ_i be dual to frame field E_1, E_2, E_3 and suppose a 1-form $\phi = \sum_i f_i \theta_i$ prove $d\phi = \sum_j (df_j + \sum_i f_i w_{ij}) \wedge \theta_j$

I'll use \det^2 & properties of \wedge and d as given in §1.6,

$$\begin{aligned}
 d\phi &= \sum_i d(f_i \theta_i) \\
 &= \sum_i (df_i \wedge \theta_i + f_i d\theta_i) \quad \text{CARTAN'S FIRST} \\
 &= \sum_{i=1}^3 \left(df_i \wedge \theta_i + f_i \sum_{j=1}^3 w_{ij} \wedge \theta_j \right) \quad \text{STRUCTURAL EQN.} \\
 &= \sum_{j=1}^3 \left[df_j + \sum_{i=1}^3 f_i w_{ij} \right] \wedge \theta_j
 \end{aligned}$$

2.) Check structural eq's of the spherical frame field,

$$\theta_1 = d\rho \quad w_{12} = \cos\phi d\theta$$

$$\theta_2 = \rho \cos\phi d\theta \quad w_{13} = d\phi \quad d\theta = w \wedge \theta$$

$$\theta_3 = \rho d\phi \quad w_{23} = \sin\phi d\theta \quad dw = w \wedge w$$

Need to check $d\theta_i = \sum_j w_{ij} \wedge \theta_j$, $dW_{ij} = \sum_k w_{ik} \wedge w_{kj}$

$$\Theta = \begin{bmatrix} d\rho \\ \rho \cos\phi d\theta \\ \rho d\phi \end{bmatrix} \quad d\theta = \begin{bmatrix} 0 \\ \cos\phi d\rho \wedge d\theta - \rho \sin\phi d\phi \wedge d\theta \\ d\rho \wedge d\phi \end{bmatrix} \quad \text{matrix notation ftw.}$$

$$W \wedge \theta = \begin{bmatrix} 0 & \cos\phi d\theta & d\phi \\ -\cos\phi d\theta & 0 & \sin\phi d\theta \\ -d\phi & -\sin\phi d\theta & 0 \end{bmatrix} \wedge \begin{bmatrix} d\rho \\ \rho \cos\phi d\theta \\ \rho d\phi \end{bmatrix} = \begin{bmatrix} \rho \cos^2\phi d\theta \wedge d\phi + \rho d\phi \wedge d\theta \\ -\cos\phi d\theta \wedge d\rho + \rho \sin\phi d\theta \wedge d\phi \\ -d\phi \wedge d\rho + 0 + 0 \end{bmatrix}$$

$$W \wedge W = \begin{bmatrix} 0 & \cos\phi d\theta & d\phi \\ -\cos\phi d\theta & 0 & \sin\phi d\theta \\ -d\phi & -\sin\phi d\theta & 0 \end{bmatrix} \begin{bmatrix} 0 & \cos\phi d\theta & d\phi \\ -\cos\phi d\theta & 0 & \sin\phi d\theta \\ -d\phi & -\sin\phi d\theta & 0 \end{bmatrix} = \begin{bmatrix} 0 & -\sin\phi d\theta \wedge d\phi & 0 \\ -\sin\phi d\theta \wedge d\phi & 0 & -\cos\phi d\theta \wedge d\phi \\ 0 & -\cos\phi d\theta \wedge d\phi & 0 \end{bmatrix} \quad \text{simplifies to } d\theta$$

$$dW = \begin{bmatrix} 0 & -\sin\phi & 0 \\ \sin\phi & 0 & \cos\phi \\ 0 & -\cos\phi & 0 \end{bmatrix} d\phi \wedge d\theta \quad \xleftrightarrow{\text{:(:)} \text{:(:)}} \begin{bmatrix} 0 & -\sin\phi & 0 \\ \sin\phi & 0 & \cos\phi \\ 0 & -\cos\phi & 0 \end{bmatrix} d\phi \wedge d\theta$$

§ 2.8 #3) Let $E_1, E_2, E_3 = \hat{r}, \hat{\theta}, \hat{z}$

- (a.) use $x = r\cos\theta, y = r\sin\theta, z = z$ to derive $\Theta_1 = dr, \Theta_2 = r d\theta, \Theta_3 = dz$.
- (b.) deduce $E_1[r] = 1, E_2[\theta] = \frac{1}{r}, E_3[z] = 1$ and others are trivial (6)
- (c.) Let $f = f(r, \theta, z)$ show $E_1[f] = \frac{\partial f}{\partial r}, E_2[f] = \frac{1}{r} \frac{\partial f}{\partial \theta}, E_3[f] = \frac{\partial f}{\partial z}$.

$$\begin{aligned} (a.) \quad E_1 &= \cos\theta U_1 + \sin\theta U_2 \quad \rightarrow \quad \Theta_1 = \cos\theta dx + \sin\theta dy \stackrel{*}{=} dr \\ E_2 &= -\sin\theta U_1 + \cos\theta U_2 \quad \rightarrow \quad \Theta_2 = -\sin\theta dx + \cos\theta dy \stackrel{**}{=} r d\theta \\ E_3 &= U_3 \quad \rightarrow \quad \Theta_3 = dz \end{aligned}$$

$$\begin{aligned} \text{To see * and ** note } r^2 &= x^2 + y^2 \Rightarrow 2rdr = 2x dx + 2y dy \\ &\Rightarrow \underline{dr = \cos\theta dx + \sin\theta dy}. \end{aligned}$$

Likewise, for **,

$$\begin{aligned} \tan\theta &= \frac{y}{x} \\ \hookrightarrow \sec^2\theta d\theta &= \frac{x dy - y dx}{x^2} \\ \hookrightarrow r d\theta &= \frac{\cos^2\theta}{r^2 \cos^3\theta} (r^2 \cos\theta dy - r^2 \sin\theta dx) \\ &\Rightarrow \underline{rd\theta = \cos\theta dy - \sin\theta dx}. \end{aligned}$$

$$(b.) \quad E_1[r] = dr(E_1) = (\cos\theta dx + \sin\theta dy)(\cos\theta U_1 + \sin\theta U_2) = \cos^2\theta + \sin^2\theta = 1.$$

$$E_2[\theta] = d\theta(E_2) = \left(\frac{-\sin\theta dx + \cos\theta dy}{r} \right) (-\sin\theta U_1 + \cos\theta U_2) = \frac{1}{r} (\sin^2\theta + \cos^2\theta) = \frac{1}{r}.$$

$$E_3[z] = dz(E_3) = dz(U_3) = 1.$$

These were correct, but there is better way, $\Theta_i(E_j) = \delta_{ij}$

$$E_1[r] = dr[E_1] = \Theta_1[E_1] = \delta_{11} = 1.$$

$$E_2[\theta] = d\theta[E_2] = \frac{1}{r}(rd\theta)[E_2] = \frac{1}{r} \Theta_2[E_2] = \frac{1}{r}.$$

$$E_3[z] = dz[E_3] = \Theta_3[E_3] = 0.$$

$$E_1[\theta] = d\theta[E_1] = \frac{1}{r} \Theta_2[E_1] = 0$$

$$E_1[z] = dz[E_1] = \Theta_3[E_1] = 0$$

$$E_2[r] = dr[E_2] = \Theta_1[E_2] = 0$$

$$E_2[z] = dz[E_2] = \Theta_3[E_2] = 0$$

$$E_3[r] = dr[E_3] = \Theta_1[E_3] = 0$$

$$E_3[\theta] = d\theta[E_3] = \frac{1}{r} \Theta_2[E_3] = 0$$

§2.8 #3 continued

(HS7)

$$(c.) E_1[f] = \cos\theta U_1[f] + \sin\theta U_2[f]$$

$$= \frac{\partial x}{\partial r} \frac{\partial f}{\partial x} + \frac{\partial y}{\partial r} \frac{\partial f}{\partial y}$$

$$= \underline{\frac{\partial f}{\partial r}}.$$

$$x = r\cos\theta, y = r\sin\theta$$

$$E_2[f] = -\sin\theta U_1[f] + \cos\theta U_2[f] \quad \begin{cases} \frac{\partial x}{\partial \theta} = -r\sin\theta \\ \frac{\partial y}{\partial \theta} = r\cos\theta \end{cases}$$

$$= \frac{1}{r} \left(\frac{\partial x}{\partial \theta} \frac{\partial f}{\partial x} + \frac{\partial y}{\partial \theta} \frac{\partial f}{\partial y} \right) \quad \begin{cases} \frac{\partial x}{\partial \theta} = -r\sin\theta \\ \frac{\partial y}{\partial \theta} = r\cos\theta \end{cases}$$

$$= \underline{\frac{1}{r} \frac{\partial f}{\partial \theta}}.$$

I leave $E_3[f] = \frac{\partial f}{\partial z}$ to reader (ii)

(4.) Frame Fields For \mathbb{R}^2 : Let E_1, E_2 form frame field on \mathbb{R}^2 then \exists angle function ψ such that

$$E_1 = \cos\psi U_1 + \sin\psi U_2 \quad (a.) \text{ find connection form and dual forms}$$

$$E_2 = -\sin\psi U_1 + \cos\psi U_2 \quad (b.) \text{ in terms of } x, y \text{ what are strct. eq's?}$$

Let $E_3 = U_3$ so we may apply the techniques of \mathbb{R}^3 w/o Δ .

$$\Theta_1 = \cos\psi dx + \sin\psi dy$$

$$\Theta_2 = -\sin\psi dx + \cos\psi dy$$

$$\Theta_3 = dz$$

$$A = \begin{bmatrix} \cos\psi & \sin\psi & 0 \\ -\sin\psi & \cos\psi & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$W = dA A^T = d\psi \begin{bmatrix} -\sin\psi & \cos\psi & 0 \\ -\cos\psi & -\sin\psi & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} \cos\psi & -\sin\psi & 0 \\ \sin\psi & \cos\psi & 0 \\ 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} 0 & d\psi & 0 \\ -d\psi & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

Structure Eq's:

$$d\Theta = W \wedge \Theta \rightarrow \begin{bmatrix} 0 & d\psi \\ -d\psi & 0 \end{bmatrix} \begin{bmatrix} \cos\psi dx + \sin\psi dy \\ -\sin\psi dx + \cos\psi dy \end{bmatrix} = \underbrace{\begin{bmatrix} -\sin\psi d\psi dx + \cos\psi d\psi dy \\ \cos\psi d\psi dx - \sin\psi d\psi dy \end{bmatrix}}_{\text{precisely } d\Theta}$$

$$W \wedge W = \begin{bmatrix} 0 & d\psi \\ -d\psi & 0 \end{bmatrix} \wedge \begin{bmatrix} 0 & d\psi \\ d\psi & 0 \end{bmatrix} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix} \not\propto dW$$

Remark: you can find the same working with 3×3 matrices...

Comment on 4

we found for arbitrary ψ that

$$E_1 = \cos \psi U_1 + \sin \psi U_2$$

$$E_2 = -\sin \psi U_1 + \cos \psi U_2$$

$$E_3 = U_3$$

The connection form is

$$\omega = \begin{bmatrix} 0 & d\psi & 0 \\ -d\psi & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

this is a bit interesting as $\psi = \tan^{-1}(y/x)$ gives polar coordinate θ (for half of \mathbb{R}^3 anyway) but, it seems we could just as well set $\psi = x^2 + y^2$ and then $\omega = \begin{bmatrix} 0 & 2x dx + 2y dy & 0 \\ -2x dx - 2y dy & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$ what would nonstandard ψ even mean? For example, $\psi = z$.

$$\begin{array}{ccc} E_1, E_2, E_3 & \xrightarrow{z=0} & U_1, U_2, U_3 \\ & \searrow \xrightarrow{z=\pi/2} & U_2, -U_1, U_3 \\ & \searrow \xrightarrow{z=\pi} & -U_1, -U_2, U_3 \\ & & \text{etc...} \end{array}$$